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1 **The role of tributary relative timing and sequencing in controlling large floods**

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8

9 **Abstract**

10 Hydrograph convolution is a product of tributary inputs from across the watershed.  
11 The time-space distribution of precipitation, the biophysical processes that control  
12 the conversion of precipitation to runoff and channel flow conveyance processes, are  
13 heterogeneous and different areas respond to rainfall in different ways. We take a  
14 sub-watershed approach to this and account for tributary flow magnitude, relative  
15 timing and sequencing. We hypothesise that as the scale of the watershed increases  
16 so we may start to see systematic differences in sub-watershed hydrological  
17 response. We test this hypothesis for a large flood ( $T > 100$  years) in a large  
18 watershed in northern England. We undertake a sensitivity analysis of the effects of  
19 changing sub-watershed hydrological response using a hydraulic model. Delaying  
20 upstream tributary peak flow timing to make them asynchronous from downstream  
21 sub-watersheds reduced flood magnitude. However, significant hydrograph  
22 adjustment in any one sub-watershed was needed for meaningful reductions in stage  
23 downstream, although smaller adjustments in multiple tributaries resulted in  
24 comparable impacts. For larger hydrograph adjustments, the effect of changing the  
25 timing of two tributaries together was lower than the effect of changing each one  
26 separately. For smaller adjustments synergy between two sub-watersheds meant the  
27 effect of changing them together could be greater than the sum of the parts. Thus,  
28 this work shows that whilst the effects of modifying biophysical catchment properties  
29 diminishes with scale due to dilution effects, their impact on relative timing of  
30 tributaries may, if applied in the right locations, be an important element of flood  
31 management.

32

33 **Key Words**

34 **Flood magnitude, sub-watershed interactions, relative timing, hydraulic**  
35 **modelling, flood risk management.**

36

37 **Introduction**

38 It is generally argued that the magnitude and frequency of river flooding is increasing  
39 throughout the world (Douglas et al., 2000; Robson, 2002; Hannaford and Marsh,  
40 2007; Petrow and Merz, 2009; Cunderlik and Ouarda, 2009; Delgado et al., 2010),  
41 and that possible climate changes (Huntington, 2006) may exacerbate this trend.  
42 Whilst attempting to slow the rate of climate change associated with human impacts  
43 has been identified as a necessary mitigation measure, it is increasingly recognised  
44 that adaptation to possible future hydrological extremes will be required  
45 (Quevauviller, 2011). Such adaptation can include reducing exposure and  
46 vulnerability to river flood events. But, it may also include adaptation of the  
47 biophysical properties of watersheds, more colloquially known as 'land management'  
48 as a means of reducing flood magnitude and hence flood risk. The reduction is  
49 delivered through changes in the attenuation of river flow, so as to reduce the peak  
50 flow in geographically-delimited areas of concern during a significant flood event.  
51 Attenuation is thought to be augmented (see summary in Lane *et al.*, 2007) through  
52 changes in water balance at the watershed scale (e.g. increases in  
53 evapotranspiration losses), changes in the timing of delivery of runoff from hillslopes  
54 (e.g. slowing the rate of runoff) or increases in temporary or permanent storage  
55 within rivers and floodplains (e.g. through encouraging flood inundation in areas  
56 where flooding might serve ecosystem benefits, such as wetlands). Management of  
57 biophysical properties in this way may be linked to ideas regarding ecosystem  
58 restoration (Maltby and Acreman, 2011) under the assumption that in less degraded  
59 landscapes (e.g. natural woodland cover; more tightly coupled river-floodplain  
60 systems; undrained wetlands), flow attenuation is naturally greater.

61 This paper is concerned with a commonly overlooked element of the management of  
62 biophysical properties in river flood management: the question of scale. Scale has  
63 been well-recognised as a critical variable in governing watershed hydrological

64 response. Notably, Blöschl *et al.* (2007) contrasted climate and land use change  
65 impacts upon high river flows. They argued that, except for the very largest  
66 watersheds, climatic changes are likely to impact entire watersheds. However, land  
67 use changes are likely to be more local in impact, with the magnitude of this impact  
68 decreasing with increasing scale. It follows that there is a critical spatial scale at  
69 which land use change impacts switch from being detectable to being undetectable.  
70 Identification of this switch is important in identifying those spatial scales at which  
71 management of biophysical watershed properties remains a viable option for  
72 reducing flood magnitude and hence flood risk.

73 A critical control on the process of attenuation is the spatial organisation of the  
74 drainage watershed. Downstream hydrographs are a convolution of the spatial and  
75 temporal variations in flow inputs from throughout the watershed (Cudennec *et al.*,  
76 2002), known as the concept of the geomorphological unit hydrograph (Rodriguez-  
77 Iturbe and Valdes, 1979). This accounts for the travel time of the flow from different  
78 parts of the watershed. The travel time is dependent upon both the geometry of the  
79 network structure and the flow hydraulics (Snell and Sivapalan, 1994), responsible  
80 for both geomorphological (Rinaldo *et al.*, 1991) and hydrodynamic (Lighthill and  
81 Whitham, 1955) dispersion. Hydrodynamic dispersion accounts for the concept that  
82 precipitation falling on the same location at the same time may not reach the outlet at  
83 the same time. This is due to flow resistance caused by friction and attenuation  
84 caused by storage. Geomorphological dispersion explains how precipitation at the  
85 same time falling on different parts of the watershed arrives at the outlet at different  
86 times. This is caused by differential flow path lengths. These principles assert that  
87 the flood wave celerity remains spatially constant during an event, particularly when  
88 bankfull discharge (the discharge when the water elevation reaches the height of the  
89 banks) (Williams, 1978) is achieved. However, Saco and Kumar (2002) dispute this  
90 assumption stating that flow velocities exhibit non-linearity in different parts of the  
91 river network. The fact that the flood wave celerity varies spatially throughout the  
92 network and over time introduces a third type of dispersion on the network travel  
93 times: kinematic dispersion.

94 Different sub-watersheds will respond to rainfall in different ways due to differing  
95 watershed characteristics, in terms of both volume and rate of runoff. The  
96 synchronicity and sequencing of tributaries inflow to the main river is further

97 complicated by the meteorological storm track. Singer and Dunne (2004) give an  
98 example where winter frontal rainfall results in flood conditions in certain sub-  
99 watersheds but others are unaffected. Yet, it is this synchronicity that will be critical  
100 to attenuation: for example, if two tributary peak flows are coincident then the  
101 magnitude of river flow is increased, while if the sub-watershed peak flows are de-  
102 synchronised then this increase is likely to be smaller (Thomas and Nisbet, 2007).  
103 Figure 1 illustrates two cases; (a) when a tributary peaks significantly before the  
104 main river and so doesn't contribute to the flood peak downstream, and (b) when the  
105 peaks of the tributary and main river are much closer, meaning that the tributary  
106 does contribute to the peak flow downstream, and is higher in magnitude. It follows  
107 that if a particular land use in a given tributary is shown to influence high flows at one  
108 particular spatial scale, the extent to which this might impact larger spatial scales  
109 depends upon the location of that tributary with respect to other tributaries and may  
110 vary between hydrological events according to how the sequencing of storm tracks  
111 impacts upon tributary response. Impacts upon both flow magnitude and the timing  
112 of response will be critical.

113 Relatively few studies have quantified the effect of localised changes in watershed  
114 biophysical properties upon tributary timing and how this impacts upon downstream  
115 river flows. Acreman *et al.* (2003) for the River Cherwell in Oxfordshire U.K. found  
116 that both floodplain storage and channel restoration had the potential to attenuate  
117 flood hydrographs, but with only a negligible impact on peak flow magnitude and a  
118 greater impact on peak flow timing. JBA (2007) considered two tributaries  
119 responsible for flooding of the River Ure at Ripon, North Yorkshire, U.K.. They  
120 recognised that the timing of the flood peaks and how the flows combined in the  
121 main river would influence the magnitude of the flood downstream. They found that  
122 whilst certain land management measures could significantly change flows in  
123 headwater basins, the impacts at larger scales were highly dependent upon the  
124 precise land management scenario and location of implementation. Thomas and  
125 Nisbet (2007) found that planting riparian woodland increased flood storage by 15-71%  
126 and that flood peaks could be delayed by 30 to 140 minutes as a result. In theory,  
127 this could either desynchronise or resynchronise tributary response according to  
128 where in a tributary, and in which tributary, the riparian woodland is planted. Lane  
129 and Milledge (2012) showed using a numerical model that whilst drainage of an

130 upland watershed increased the rate of runoff and hence the timing of maximum flow  
131 in a flood event, it did not impact the level of runoff concentration and hence flood  
132 flow magnitude. Whilst the watershed response was marginally earlier, the impacts  
133 of this response upon downstream flood risk depended upon how this response  
134 changed with respect to other sub-watersheds: the impacts of changing biophysical  
135 properties were relative and scale dependent.

136 In this paper, we take a different approach to the question of tributary timing effects.  
137 We focus upon a major river flood in a large watershed (c. 2,400 km<sup>2</sup>) in the north of  
138 England and use, primarily, numerical simulation to quantify how changes in tributary  
139 timing impact upon downstream flood magnitude. We aim to test the hypothesis that  
140 the timing of tributary response, a function of both the static organisation of the  
141 watershed drainage network and the dynamic of individual flood events, can exert a  
142 significant impact upon downstream flood magnitude and hence flood risk. Our  
143 approach compliments statistical approaches (Lane, 2003; Pattison *et al.*, in review)  
144 that have shown for high river flows (with a daily discharge frequency of less than  
145 1%, including flood flows), substantial flow variability can be explained by differences  
146 in the relative timing of flow peaks.

147

## 148 **Methodology**

### 149 *Eden Watershed*

150 The focus of this paper is a major flood event (January 2005) in the city of Carlisle,  
151 on the River Eden in Cumbria U.K. The Eden watershed has an area of 2,400 km<sup>2</sup>  
152 and an average annual precipitation of 1,183 mm a<sup>-1</sup> (Environment Agency, 2008). It  
153 consists of 6 major sub-watersheds; the Upper Eden, Eamont, Irthing, Caldew,  
154 Petteril and main lower Eden (Figure 2). The Upper Eden at Temple Sowerby is the  
155 largest sub-watershed (616.4 km<sup>2</sup>) and has several tributaries originating in the  
156 Howgill Fells and the Pennines. The River Eamont drains from the English Lake  
157 District and receives the highest rainfall in the whole watershed (1768 mm yr<sup>-1</sup>) and  
158 has geology of metamorphic volcanic rocks, which are very impermeable and lead to  
159 rapid runoff (Environment Agency, 2008). This sub-watershed is heavily regulated  
160 by the attenuating effect of Ullswater lake and the reservoir of Haweswater. The

161 Irthing is the only main right bank tributary draining from the Northern Pennines and  
162 Border mires and is dominated by forestry. The Petteril is a lowland river and its  
163 watershed has improved pasture and arable agriculture as its main land use. This  
164 sub-watershed experiences the lowest rainfall totals with 942 mm a<sup>-1</sup>. Finally, the  
165 Caldew drains from the highest topography region in the watershed, the Skiddaw  
166 fells of the Lake District (950m AOD) and consists of impermeable volcanic geology.  
167 The Eden watershed is therefore particularly diverse in terms of its climate,  
168 topography, soil types, geology, and land cover (Environment Agency, 2008). This  
169 means that the drivers of watershed scale flood risk are spatially variable, as  
170 rainfall/runoff inputs and response times are spatially variable.

171 The focus of this paper is the January 2005 flood event was the most extreme the  
172 watershed has ever experienced in the historical and measured record (Archer *et al.*,  
173 2007a; 2007b) dating back to 1770 which was reconstructed by Pattison and Lane,  
174 (2012a), with the flood level in Carlisle being 1 m higher than the previous worst  
175 flood on record (Environment Agency, 2006). The storm event that caused this  
176 flooding extended from the 6<sup>th</sup> to the 9<sup>th</sup> January 2005 and affected Northern  
177 England, Southern Scandinavia, Germany and the Baltic Region. The extreme  
178 nature of the event is linked to its duration, rather than the intensity of the rainfall.  
179 Overall, this storm has been estimated as having a return period of 50-100 years  
180 (0.02-0.01 annual probability) but resulted in a flood on the River Eden with a return  
181 period of greater than 100 years. The most significant rainfall was orographically-  
182 forced, in the south of the watershed. Wet Sleddale in the Eamont sub-watershed  
183 recorded 207mm rainfall over the three days of the event, with a return period  
184 estimated at c.170 years (0.58%). This rainfall resulted in an extreme hydrological  
185 response, with all river systems experiencing high flows demonstrating the spatially  
186 extensive high magnitude rainfall experienced in this event, rather than the effects  
187 localised high intensity precipitation. A total of 2016 properties were flooded  
188 throughout the watershed, of which 1865 were in the city of Carlisle. The total  
189 economic cost of the flood was between £350 million and £400 million (Environment  
190 Agency, 2006) at 2005 prices.

191 *Statistical*

192 To assist with the interpretation of the hydraulic model results, a dataset of 134 high  
193 flow events were obtained from the Sheepmount gauging station in Carlisle (Figure  
194 2), for the period 1977-2007. These were defined as events that exceed the  
195 threshold of  $347 \text{ m}^3\text{s}^{-1}$ , corresponding to a frequency of 1% or less in terms of daily  
196 mean flow. These data have been subject to an intensive statistical analysis  
197 (Pattison *et al.*, in review), focusing upon the magnitude and timing of peak high  
198 flows (and not just floods). Relative timing was calculated by subtracting the time of  
199 the peak flow in the sub-watershed from the time of peak flow downstream in the  
200 main Lower Eden at Carlisle. Here, we use this dataset to contextualise the 2005  
201 flood. Initial analysis showed that the January 2005 flood event was significantly  
202 different to all other 134 events in this record, with the peak discharge ( $1516 \text{ m}^3\text{s}^{-1}$ )  
203 through the city of Carlisle being 304% of the long term average of the peak-over-  
204 threshold (POT) events between 1977 and 2007, and so additional analyses were  
205 employed to try and explain this difference. Firstly, the average peak discharge was  
206 calculated for all the tributaries and the main stem. The deviation from this average  
207 was calculated for the January 2005 event, and expressed as a percentage. This  
208 was done in terms of both peak magnitudes and relative timing. Second, the relative  
209 timing of the peak flows is affected by both the speed of the flood wave and the  
210 distance between the sub-watershed and Carlisle. Therefore, the speed of flood  
211 wave propagation, wave celerity ( $C$ ) is calculated from:

$$C = \delta x / \delta t$$

[2]

214 where:  $\delta x$  is the longitudinal distance; and  $\delta t$  is the time difference. Use of these  
215 basic data helped to contextualise the January 2005 event.

216

### 217 *Hydraulic Modelling*

218 A watershed scale hydraulic model, which incorporates the major tributaries of the  
219 Upper Eden, Eamont, Irthing, Petteiril and Caldew was constructed in iSIS-Flow, a  
220 standard 1D hydraulic model (Halcrow, iSIS Guide). iSIS-Flow can be applied to  
221 open channel systems where discharge and stage can be simulated. Hydraulic units  
222 such as channel cross sections and structures e.g. bridges and weirs form the basis



223 of the model structure, with upstream and downstream boundary conditions  
224 necessary to initiate a hydrograph and convert stage to discharge respectively.  
225 Confluences are represented by junction units which are governed by the continuity  
226 of flow and equality of water surface level equations (iSIS Manual, Halcrow). The  
227 iSIS-Flow model was modified from an existing hydraulic model developed for the  
228 Environment Agency of England and Wales for the Eden (Atkins, 2005). The  
229 upstream boundary condition for each tributary was the respective hydrograph from  
230 the January 2005 flood event. The model was validated using gauged data from the  
231 Sheepmount, Linstock and Great Corby gauging stations. Calibration for this event  
232 was optimised by the peak stage at Sheepmount. Figure 3a shows the process by  
233 which the model was calibrated. The Manning's  $n$  roughness parameter was  
234 changed within, before or after Carlisle. Increasing Manning's  $n$  will increase the flow  
235 resistance meaning that stage increases locally for a given discharge. Therefore  
236 when  $n$  is increased downstream of Carlisle water is backed-up and stage increases  
237 in the centre of Carlisle. The optimum calibrated model was achieved through  
238 increasing  $n$  by 0.01 within and before Carlisle (Figure 3b). The performance of the  
239 calibrated model is indicated by the following statistics; (a) percentage error in  
240 predicted flow magnitude of -1.5% (equivalent to -0.20 m of flow stage) and +0.03%  
241 in flow timing (1.25 hours); (b) Nash Sutcliffe Coefficient = 0.85; (c) RMSE = 0.67m;  
242 and (d) % error in volume = 5.2%).

243 Internal model validation was also assessed at two other gauging stations. At Great  
244 Corby the model also performs relatively well, with an error of 0.079 m and 0.83  
245 hours on the magnitude and timing of the peak stage. This corresponded to a 1.8%  
246 error in terms of peak discharge. However, at Linstock the model performs less well,  
247 with an error of 0.59 m and 1.83 hours. The difficulty in using this stations gauged  
248 data are highlighted by two limitations. Firstly, there were problems with the  
249 recording of the event at Linstock, with instrumentation failing during the event just  
250 after the peak stage. Secondly, there is no rating curve at Linstock to assess the  
251 effect on flow. The errors reported here provide a qualitative indication of the  
252 magnitudes of change in predicted flow necessary during the experiment for there to  
253 be some confidence that real changes are being identified.

254 The general approach to the hydraulic modelling experiment consisted of changing  
255 tributary input systematically in terms of both the magnitude (0.5%, 1%, 2%, 5%,

256 10%, 15%, 20%, 25% reductions) of the flows and the timing (15 minutes, 30  
257 minutes, 1 hour, 2 hours, 3 hours, 4 hours, 6 hours, 8 hours earlier and later) of the  
258 flows for individual tributaries. In practice, the process of attenuation does not  
259 function by just delaying and reducing the peak flow, it changes the shape of the  
260 hydrograph. Therefore, the hydrograph was also be stretched in the terms of time  
261 and squashed in terms of flow magnitude simultaneously, through using change  
262 factors:

$$263 \quad \textit{Magnitude} = \textit{Original} \times \textit{Change factor}$$

$$264 \quad \textit{Time} = \textit{Original} \div \textit{Change factor}$$

265 [1]

266 Use of these change factors, unlike simple changes in magnitude and timing,  
267 conserves flood volume whilst changing attenuation.

268 Scenarios involving more than one of the major tributaries were also tested, and  
269 experiments were undertaken that included both timing and magnitude shifts from  
270 the same tributary simultaneously. This was because it is hypothesised that it may  
271 be easier to change the flows from more than one sub-watershed by a smaller  
272 amount and still achieve the same effect as shifting one sub-watershed by a large  
273 amount.

## 274 **Results**

### 275 *The 2005 event in a statistical context*

276 The peak discharge through the city of Carlisle as measured by the Sheepmount  
277 gauging station was  $1516 \text{ m}^3\text{s}^{-1}$ , 304% of the long term average of the POT events  
278 between 1977 and 2007 (those  $>347 \text{ m}^3\text{s}^{-1}$ ) (Figure 4a). Possible causes for this  
279 extreme flood in terms of the contributing sub-watersheds are that: (1) a specific sub-  
280 watershed had an extreme response to rainfall and caused a large flood downstream;  
281 or (2) that all the sub-watersheds responded with greater than average peak flows;  
282 or (3) that individual tributary responses were synchronised. The data show that the  
283 Petteril tributary deviated most from the long-term average, with a 2005 peak  
284 magnitude on the Petteril being 335% of the long-term average. However, this was  
285 still the lowest actual contribution ( $82.6 \text{ m}^3\text{s}^{-1}$ ) from any of the major sub-watersheds.

286 The Irthing contribution was 282% of the long term average, while the contribution  
287 from the Caldew (187%), Eamont (215%) and Upper Eden (Kirkby Stephen = 209%,  
288 Temple Sowerby = 187%) were all about double the long term average peak flow.  
289 This highlights the importance of scale in causing extreme floods in this example: all  
290 sub-watersheds were contributing large flows, associated with a synoptically  
291 coherent rainfall event. The sum of the contributing tributary peak discharges for the  
292 2005 event was  $1239 \text{ m}^3\text{s}^{-1}$  which is 18.3% lower than the actual peak discharge  
293 downstream in Carlisle. This suggests a high level of tributary synchronicity as the  
294 sum of the average tributary peak discharges is  $581.7 \text{ m}^3\text{s}^{-1}$  which is 16% greater  
295 than the average flood discharge in Carlisle.

296 The question that remains is the extent to which the effects of synoptic coherence  
297 were exacerbated by the relative timing of response of the major tributaries, with  
298 respect to the downstream gauging station of Sheepmount in Carlisle: to what extent  
299 does interaction of the flows from each sub-watershed (i.e. synchronicity),  
300 exacerbate the effects of tributary synchronicity? The timing of the Eamont was not  
301 significantly different to the long term average (107%) (Figure 4b). However, the  
302 timing of the Upper Eden was earlier than in the long term average flood by 4-5  
303 hours. This meant that the sequencing of the Eamont and Upper Eden was switched  
304 around, so that the Upper Eden peaked much earlier and much closer in time to the  
305 Eamont. Due to the proximity of the gauging stations on each of these rivers, it can  
306 be assumed that peak flows coincided and flowed down the Middle Eden together.  
307 Table 1 shows that both these tributaries had a higher flood wave celerity than the  
308 other tributaries. This makes it likely that the peak flow from the upstream sub-  
309 catchments were synchronous with the lower sub-catchments peak flows resulting in  
310 this extreme downstream flood.

311 The Petteril also seemed to peak significantly earlier (7 hours) than during other  
312 smaller floods with respect to the flow gauge at Sheepmount in Carlisle. The Petteril  
313 also peaks earlier with respect to the all other sub-watersheds. These changes  
314 combined to reverse the sequencing of flow combination in and upstream of Carlisle.  
315 Normally, the Petteril peaks just after the Eden, and the flows combine in Carlisle. In  
316 the 2005 event, the Petteril peaked about 3.75 hours before the main Eden,  
317 maintaining high flows in Carlisle for a longer period, but the discharge was not as  
318 high as would have occurred under the normal situation, with the Petterill peaking

319 just after the Eden. All other sub-watersheds peaked earlier than during the long  
320 term average flood, but the sequencing stayed the same. This evidence emphasises  
321 that synchronicity is a complex relative process: the change in timing of the Upper  
322 Eden may have exacerbated the peak flow magnitude at Carlisle, but the earlier  
323 response of the Petteril may have reduced it.

324 Relative timing can also be considered in terms of the celerity of the flood wave.  
325 Table 1 compares the mean wave speed propagation rates downstream (celerity) to  
326 the celerity of the flood waves from the different tributaries for the January 2005 flood  
327 event. First, considering how different tributaries compare to each other in the  
328 average event, it is clear that the upper sub-watersheds (Upper Eden and Eamont)  
329 have significantly higher flood wave celerity than the lower sub-watersheds (Irthing,  
330 Petteril and Caldew), and reflecting the steeper valley slopes of the upper sub-  
331 watersheds. The reduction in mean wave celerity calculated for Warwick Bridge to  
332 Carlisle reflects the onset of significant attenuation from Temple Sowerby  
333 downstream, reflecting the onset of floodplain storage, known to occur from the  
334 Middle Eden (Temple Sowerby) downstream.

335 Second, during the January 2005 flood event, the propagation of the flood wave from  
336 each of the tributaries was slower than during the average flood event, by a  
337 significant degree (>40%) in most cases. The major exception is the lowest reach  
338 (downstream of Warwick Bridge) which had a very similar flood wave celerity to the  
339 average event. Knight and Shiono (1996) investigated the effect on flood wave  
340 celerity of in-channel and out-of-bank flows, showing that lag time decreases (and  
341 celerity increases) with increasing in-channel discharges and lag time increases  
342 (celerity decreases) once out-of-bank discharge begins. Table 1 implies that all the  
343 tributaries flood waves were experiencing out-of-bank storage and attenuation  
344 between their confluences and the city of Carlisle.

345

#### 346 *Hydraulic model results*

347 First, the effect of changing tributary discharge magnitudes on downstream (Carlisle,  
348 Sheepmount) peak stages is assessed in Figure 5. The maximum reduction in peak  
349 stage (0.33 m) in Carlisle was caused by a 25% reduction in the flows from the

350 Upper Eden. Figure 5 suggests that the Upper Eden is always the most effective at  
351 reducing downstream stage, as it has the largest flow contribution of all the sub-s in  
352 actual discharge terms. The Irthing and Eamont offer similar amounts of flood stage  
353 reduction downstream (0.25 m and 0.21 m respectively). At lower percentage flow  
354 reductions, the Eamont is more effective than the Irthing, but with greater than 10%  
355 flow reduction the Irthing becomes more beneficial. The Caldew has very little  
356 impact on peak stage in Carlisle until it is decreased by more than 10%. However,  
357 for greater than 15% flow decreases, the Caldew has no further impact on peak  
358 stage downstream in Carlisle. Reducing the flow contribution of the Petteril has very  
359 little effect on peak stage at Carlisle, with a 25% reduction in the magnitude of the  
360 Petteril flows only resulting in a 0.05 m reduction in the peak stage downstream.  
361 This is because the flows of the Petteril are lowest in actual terms.

362 It is important to take account of the error associated with the model. The baseline  
363 simulation had a 0.20 m error on the peak stage at Carlisle. To determine whether  
364 any of these change scenarios result in no out of bank flow, the error has to be  
365 subtracted from the bankfull level (solid black line). The threshold for the flow to be  
366 contained within the channel taking into account the error of the model is 13.71 m.  
367 The only magnitude change scenarios which result in a peak stage less than the  
368 bankfull are the Upper Eden 25% and 20% and the Irthing 25%.

369 Second, the effect of changing tributary peak flow timing on downstream (Carlisle)  
370 peak stages was assessed. These consisted of the hydrograph being shifted by the  
371 timings ranging from 0.25 hour to 8 hours, and the results are shown in Figure 6.  
372 The effect of changing the timing of the Petteril has a minimal effect on the peak  
373 stage. Delaying the upper sub-watersheds (Upper Eden and Eamont) reduces peak  
374 stage. When these tributaries peak earlier, peak stage increases. The longer these  
375 tributaries are delayed, the greater the reduction in peak stage downstream.  
376 Delaying these tributaries has a similar effect on peak flow in Carlisle up to a delay of  
377 6 hours with peak stage reductions of 0.24 m and 0.23 m respectively. However, a  
378 delay of 8 hours of the Upper Eden has a greater effect than the same shift on the  
379 Eamont, with a 0.32 m and 0.27 m reduction in peak stage respectively. The effect  
380 of these tributaries peaking earlier is for peak stage downstream to increase by 0.05  
381 m for the Upper Eden and 0.08 m for the Eamont.

382 The effect of speeding up the response of the Caldew by 8 hours is the same as  
383 caused by delaying the Upper Eden by 8 hours: a peak stage reduction of 0.33 m.  
384 Delaying the Caldew results in higher peak stages at Carlisle, with an increase of  
385 0.16 m with an 8 hour delay. Similar trends are shown for the Irthing, with a 0.26 m  
386 decrease in peak stage when the Irthing is speeded up by 8 hours. However, a  
387 more complex trend is evident when the Irthing is delayed. A delay of up to 4 hours  
388 leads to a slight increase in peak stage downstream, with the effect of a 1 hour delay  
389 having the greatest impact on stage. However, a delay of greater than 4 hours leads  
390 to a decrease in peak stage in Carlisle. An 8 hour delay of the Irthing results in a  
391 0.09 m decrease in peak stage downstream.

392 The error associated with the baseline model is 0.20 m error on the peak stage at  
393 Carlisle, resulting in a threshold for overbank flow of 13.71 m. It is evident that  
394 significant changes in the timing of the tributaries are needed to lead to peak stages  
395 below this threshold. Firstly, a 6 hour (13.70 m) and 8 hour (13.62 m) delay of the  
396 Upper Eden results in a peak stage in Carlisle within bank. An 8 hour delay of the  
397 Eamont is required, resulting in a peak stage of 13.67 m. Other scenarios that lead  
398 to no out of bank flow are when the Caldew peaks 6 hours (13.69 m) or 8 hours  
399 (13.61 m) earlier or the Irthing peaks 8 hours earlier (13.69 m).

400 The uncertainties associated with these scenarios were evaluated by assessing the  
401 sensitivity of the peak stage downstream to the roughness of the channel cross  
402 sections. This type of uncertainty analysis is more common and developed in the  
403 application of hydrological models rather than hydraulic models. For this reason, as  
404 well as the instability of the hydraulic model under certain parameterisations and  
405 scenarios, a basic experiment is carried out for the most extreme of the scenarios  
406 reported in this paper (i.e. 25% magnitude reduction, 8 hour delay/ earlier) for the  
407 most common calibration parameter in a hydraulic model; Mannings n for the values  
408 of +0.005, +0.01 and +0.02. Results for these simulations are shown in Figure 7a  
409 (Magnitude), 7b (Time delay) and 7b (Earlier time). The significant outcomes of this  
410 uncertainty analysis are firstly that the hydraulic model is more sensitive to Mannings  
411 roughness than it is to the hydrograph boundary conditions. The range of peak  
412 stages between the different tributary scenarios is much smaller than it is for the  
413 roughness sensitivity analysis. Secondly, as the Mannings n value increases globally  
414 throughout the whole network, the difference between the scenarios for the different

415 tributaries decreases. However, for small changes in roughness (+0.005) the relative  
416 order of the tributary scenarios stays the same. Although basic, this uncertainty  
417 analysis suggests that results are uncertain depending on the choice of Mannings n.  
418 However, the baseline value of n used in the analysis reported gives the best match  
419 with the observed gauged data, and are most physically representative for the river  
420 channel network.

421 Scenarios for multiple sub-watershed timings (Upper Eden and Eamont) were then  
422 tested. Results, in terms of the effect of timing on peak stage downstream at Carlisle  
423 are shown in Figure 8. This shows that the maximum stage reduction is achieved by  
424 a time delay of both tributaries by 8 hours in combination (0.44 m). The same effect  
425 of delaying one of the tributaries by 8 hours can be achieved by delaying both  
426 tributaries by 4 hours each (0.32 m). The combination of different timing delays from  
427 both the Eden and Eamont together sometimes provides additional benefits over  
428 when the stage reduction caused by each tributary in isolation are added together.  
429 This synergy means that smaller changes in both sub-watersheds may be equal to  
430 larger shifts from just one tributary. This is the case for the scenarios which include  
431 any time delay of one of the tributaries in addition to a lower time delay for the other  
432 ( $\leq 1$  hour for the Eden and  $\leq 0.50$  hour for the Eamont). This is important given the  
433 expected ease of achieving smaller delays through changes in watershed-scale  
434 biophysical properties. When both tributaries are delayed by larger amounts the  
435 amount of peak stage reduction in Carlisle is less than the separate effects of  
436 delaying each tributary added together. The same effect downstream can be  
437 achieved by smaller time delays of both tributaries simultaneously or a longer time  
438 delay of just one of the rivers. For example, an hour delay of the Eden results in a  
439 0.03 m reduction of the peak stage at Carlisle, while a half hour delay of both  
440 tributaries together results in a 0.03 m decrease.

441 At low time delays (< 5 hours) both tributaries are both as effective as each other in  
442 terms of the effect of delaying their flow. However, for longer delays, the impacts are  
443 variable between tributaries. In scenarios where the time delay of the Eden is high (>  
444 6 hours), downstream flood stage is more sensitive to the Eamont if it is delayed by  
445 more than 3 hours. This means that beyond 6 hours delay of the Eden, the peak  
446 stage in Carlisle decreases more per unit time delay greater than 3 hours of the  
447 Eamont than the Eden. However, in scenarios where the time delay of the Eden is

448 less than 6 hours, downstream flood stage is more sensitive to the Eden when the  
449 Eamont is delayed by more than 5 hours. This means that for a time delay of the  
450 Eden by less than 6 hours and a time delay of the Eamont by more than 5 hours, the  
451 peak stage in Carlisle decreases more per unit time delay of the Eden than the  
452 Eamont.

453 Changes in watershed-scale biophysical properties would not alter the magnitude or  
454 timing of the flow response in isolation, but the size and shape of the hydrograph in  
455 combination. Therefore, scenarios of combined magnitude and timing shifts were  
456 made for the Upper Eden and Eamont. The effect of shifts in timing and magnitude  
457 for the Upper Eden are shown in Table 2. The maximum peak stage reduction at  
458 Carlisle is 0.42 m, caused by an 8 hour delay and a 25% decrease in magnitude.  
459 For scenarios with timing delays less than 5 hours and magnitude reductions of less  
460 than 10%, the effect on downstream peak stage is equally sensitive to timing and  
461 magnitude changes in the Upper Eden. The importance of timing delays increases  
462 after 5 hours, with peak stage reduction being more sensitive to changes to timing  
463 than magnitude above this threshold. This means that beyond 5 hours delay of the  
464 Eden, the peak stage in Carlisle decreases more per unit time delay than per  
465 percentage decrease of flow magnitude. The sensitivity of downstream flood stage  
466 to magnitude shift is high for shifts greater than 20% when the Upper Eden is shifted  
467 in time by less than 5 hours. This means that changes of flow magnitude beyond 20%  
468 have a greater effect on downstream peak stage than large changes in the timing of  
469 that flow.

470 The combinations of different timing and magnitude shifts sometimes produce added  
471 benefit to both the scenarios separately. The scenarios that fit this criterion are  
472 shown in bold font in Table 2. This suggests that small time delays ( $\leq 1$  hour) in  
473 addition to any magnitude reduction combined provide more than the expected level  
474 of peak stage decrease downstream, than if either time delay or flow magnitude  
475 reduction were implemented separately. The greatest gain is for the smallest  
476 magnitude increase and smallest time delay (2% magnitude, 0.25 hours), with 0.01  
477 m extra stage decrease in Carlisle. However, for the scenarios combining larger  
478 magnitude decreases and time delays, less than the expected stage decrease is  
479 found downstream, with a 25% decrease in magnitude causing 0.33 m, and an 8



480 hour delay causing 0.32 m separately, but in combination they only cause a 0.42 m  
481 decrease in downstream peak stage instead of 0.65 m.

482 The effect of shifts in timing and magnitude for the Eamont are shown in Table 3.  
483 The maximum peak stage reduction at Carlisle is 0.38 m, caused by an 8 hour delay  
484 and a 25% decrease in magnitude. This indicates that the peak stage at Carlisle is  
485 more sensitive to changes in the flows (both magnitude and timing) of the Upper  
486 Eden than the Eamont. Downstream flood stage reduction is more sensitive to the  
487 timing than the magnitude for lower magnitude changes. This means that smaller  
488 changes in the timing of the hydrograph have a greater impact on downstream stage  
489 than changes in the magnitude of the flows from the Eamont. This is a particularly  
490 useful finding as it is expected that delivering time delays (e.g. through encouraging  
491 floodplain storage) will be easier than changing the flow magnitude through land  
492 management changes. However, for higher magnitude changes (>20%), magnitude  
493 becomes more important than the timing of the peak in impacting downstream peak  
494 stage, especially for small time delays.

495 Scenarios that combine both magnitude decreases and time delays of the Eamont  
496 have an added benefit for downstream flood stage as compared with the expected  
497 reduction from each separate scenario added together. A magnitude decrease of  
498 2%, combined with any of the timing delays, produces a peak stage downstream  
499 lower than what is expected by each individual change combined. However, for  
500 changes in magnitude greater than 2% only small time delays ( $\leq 0.50$  hour) produce  
501 more than the expected amount of peak stage reduction downstream.

502 Finally, the more physically realistic scenario of hydrograph attenuation, where the  
503 flood peak is both delayed and reduced in magnitude, with the hydrograph shape  
504 being altered, is considered. The impact of these scenarios on downstream peak  
505 stage is shown in Figure 9: the effect of attenuation of the downstream flood peak of  
506 the Upper Eden is greater than the same amount of attenuation of the Eamont,  
507 although the differences between the impact of each tributary are minor. As the  
508 amount of attenuation increases, the amount of peak stage reduction downstream  
509 increases. Furthermore, as the amount of attenuation increases, the effect of the  
510 Upper Eden diverges from the effect of the Eamont. This suggests that the Upper  
511 Eden is more effective at reducing downstream peak stage. However, while the

512 gradient of the Eamont line is reasonably constant, the Upper Eden becomes less  
513 effective for a change factor lower than 0.85. An attenuation factor of 0.891 is  
514 required for the Eamont flow to be reduced to bankfull height, even accounting for  
515 the error associated with the iSIS model. The attenuation factor is lower for the  
516 Eden, with a value of 0.873.

## 517 **Discussion**

518 The above results suggest that tributary flow magnitudes exert a considerable impact  
519 upon downstream flow magnitude. But, they also suggest that the interaction of  
520 different sub-watersheds in determining the magnitude of downstream floods has  
521 been demonstrated both in terms of synchronicity and sequencing. If tributary peak  
522 flows are closer in time to the peak discharge on the main river then the flood wave  
523 travelling downstream in the main river is larger. Furthermore, if the order in which  
524 tributary peak flows occur changes, how these interact with each other and the main  
525 river has important implications for downstream flood risk.

526 Hydrodynamic dispersion explains the propagation of disturbances to disperse  
527 longitudinally as the flood wave travels downstream (Lighthill and Whitham, 1955;  
528 Rinaldo et al., 1991). Hydrodynamic dispersion is illustrated in this analysis by the  
529 celerity of the flood wave being considerably lower during the 2005 event as  
530 compared to the average flood in the Eden. The celerity in different reaches and  
531 tributaries of the main river was also different. This follows Saco and Kumar's (2002)  
532 concept of kinematic dispersion. This suggests that peak stage reaches bankfull in  
533 some reaches/tributaries and not others. Geomorphological dispersion accounts for  
534 the river network structure in the propagation of the flood wave downstream (Rinaldo  
535 et al., 1991). The importance of geomorphological dispersion is demonstrated by  
536 changing the flows from one individual sub-watershed, whilst the other tributaries  
537 flows are kept the same, and which results in differences in the downstream peak  
538 flow magnitude. The fact that some tributaries have more/less of an effect upon the  
539 downstream discharge shows that the network structure is important. White et al.,  
540 (2004) found that as watershed size increases, network structure plays an  
541 increasingly important role in determining the watershed scale response, compared  
542 to channel hydraulics. This means that in large watersheds, where runoff in the  
543 watershed is generated is critical in explaining downstream flood risk, as

544 geomorphological dispersion overwhelms other processes operating at smaller  
545 scales. This work has found that geomorphic, kinematic and hydrodynamic  
546 dispersion are important at all spatial scales, with the downstream hydrograph being  
547 primarily dependent upon geomorphic dispersion with specific reaches being  
548 subjected to different levels of kinematic and hydrodynamic dispersion. It is  
549 therefore the drainage network structure, in combination with more localised factors  
550 of flood wave celerity and attenuation, which control the watershed scale response.

551 In this analysis, we have taken a single downstream point: a large urban centre. The  
552 watershed studied is unusual in that Carlisle is the only major city in the Eden  
553 watershed and it is almost at its most downstream location. From a flood risk  
554 management perspective, this justifies a singular focus upon one location. However,  
555 it is worth speculating as to what would be the effect in a similar watershed with a  
556 higher population density and perhaps more large urban centres. Here, it is possible  
557 that the spatial scale of the watershed that is relevant to a specific urban area  
558 changes depending upon which urban area is the focus, such that timing effects that  
559 matter at one spatial scale may cause opposing effects at other spatial scales. For  
560 instance, desynchronising two tributaries may benefit the reach immediately  
561 downstream. But if this causes one of the two tributaries to become more  
562 synchronous with a third tributary, further downstream, a reduction in flood risk for  
563 one river reach may well translate into an increase for a second river reach. This is  
564 the sense in which the effects of changing the timing of tributary response can only  
565 be judged *relative* to those downstream locations thought to be of importance for  
566 flood risk reduction. Even if the absolute benefits of a tributary timing change can be  
567 shown, and this geomorphological effect is dominant over variability in hydrodynamic  
568 effects, this absolute benefit may not hold for all scales of consideration. The  
569 complexity of watershed scale flood risk management comes from the problem of  
570 multiple areas of focus and concern, and how one measure in one location may  
571 benefit one urban area downstream but enhance flood risk in another.

572 In addition, due to temporal variation in how tributaries respond to different kinds of  
573 precipitation events, modification of the biophysical properties of watersheds is likely  
574 to be fundamentally different, as a flood risk reducing solution, to more traditional  
575 engineering solution. The same biophysical properties in one area will have different  
576 effects than in another area, depending where in the catchment they are relative to

577 the drainage network and the downstream urban centre. These effects will be  
578 specific to different storm events, depending on how the landscape interacts with the  
579 precipitation (Pattison and Lane, 2012b). Biophysical landscape properties can  
580 cause flow attenuation through changing the water balance, changing the timing of  
581 runoff delivery or through storage. How the biophysical properties of one area  
582 interacts with all the other areas within the catchment is what determines the  
583 cumulative effect downstream. Whilst this study demonstrates the significant role  
584 played by attenuation in controlling downstream flood magnitude, what is less clear  
585 and needs further attention is the impact of changing the biophysical properties on  
586 the magnitude and timing of runoff, and hence attenuation. An uncertainty over the  
587 applicability of these results comes from the uncertainty over what proportion of flow  
588 magnitude reduction can be achieved through land management changes. Can this  
589 be as high as 25%? A recent study by Wheeler et al (2008) suggest yes, with  
590 shelterbelts and full woodland cover resulting in a 29% and 50% reduction in peak  
591 flows in the Pontbren catchment, and 5% and 36% in the Eden catchment for the  
592 January 2005 flood event used in this paper. The second question is how much can  
593 upstream land management slow the flow? Far less research has been done on this  
594 aspect and therefore the answer is highly uncertain. Odoni and Lane (2011) found  
595 that in channel woody debris could result in up to 3 hrs delay. However, the study by  
596 Acreman et al (2003) found that channel restoration could delay flood peaks by up to  
597 17 hours.

## 598 **Conclusion**

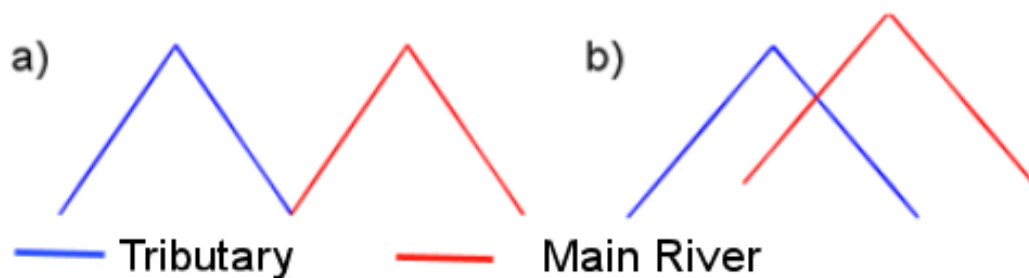
599 This paper provides evidence for the important role of the drainage network structure  
600 in controlling large floods. The case study of the River Eden in the English Lake  
601 District, and the extreme January 2005 flood event, is used to demonstrate this  
602 principle. Numerical experiments were carried out using a 1D hydraulic model, iSIS,  
603 whereby the sensitivity of downstream flood magnitude to each tributaries  
604 hydrograph was assessed. Scenarios included changing single tributary flow  
605 magnitudes and timing, as well as for multiple tributaries simultaneously.  
606 Furthermore, this provides evidence for how localised changes in watershed  
607 biophysical properties can result in very different downstream impacts depending on  
608 where they originate in the wider watershed. The dominant processes differ between  
609 scales, making it unlikely that relationships observed at one scale (e.g. the field) are

610 the same at a larger spatial scale (e.g. the watershed). At the watershed-scale the  
611 role of tributary relative timing and synchronisation is important in determining the  
612 magnitude of the flood peak downstream. For the single flood event considered here,  
613 it was shown that with different kinds of sub-watershed response it was possible to  
614 reduce the magnitude and duration of our-of-bank flows, almost eliminating them in  
615 some scenarios. But, this conclusion also reveals a problem: even if the changes in  
616 sub-watershed response can be delivered, the desired sub-watershed response is  
617 likely to vary with the space-time distribution of extreme rainfall events.

618 **Acknowledgements**

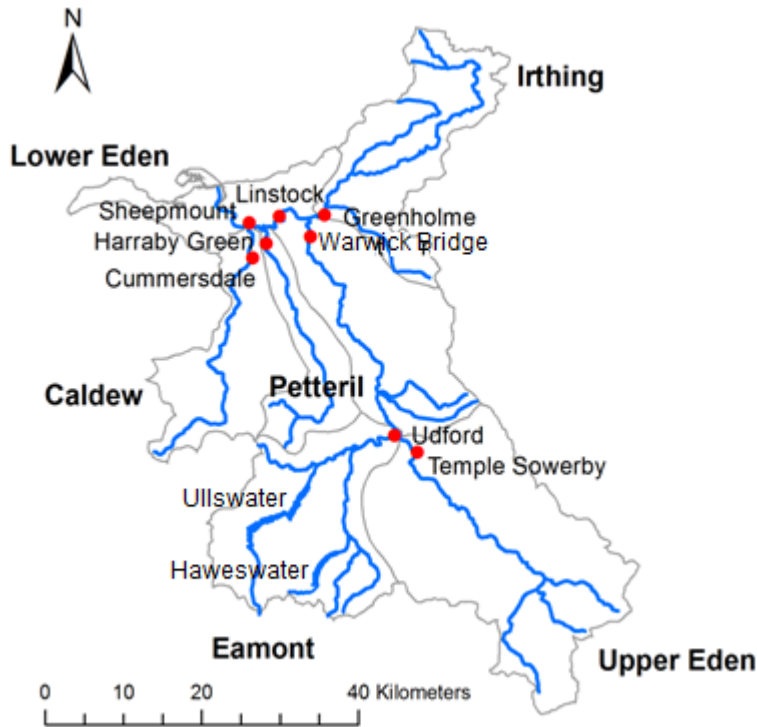
619 This research was funded by Environment Agency and United Utilities as part of the  
620 EU Interreg IVB project ALFA (<http://www.alfa-project.eu>); acknowledges additional  
621 support came from Durham University and the Eden Rivers Trust.

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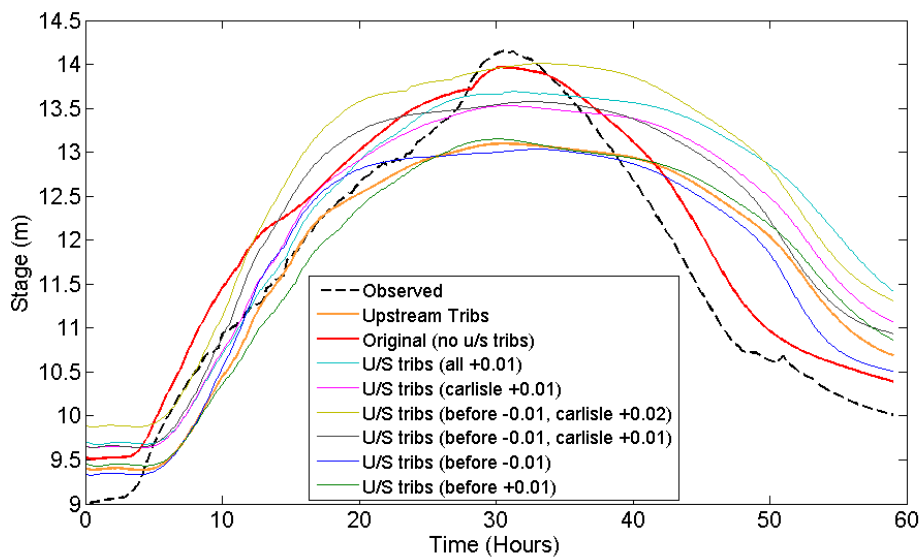
624 **Figure 1** *Effect of tributary synchronicity with respect to the main river on*  
625 *downstream peak flow magnitudes.*

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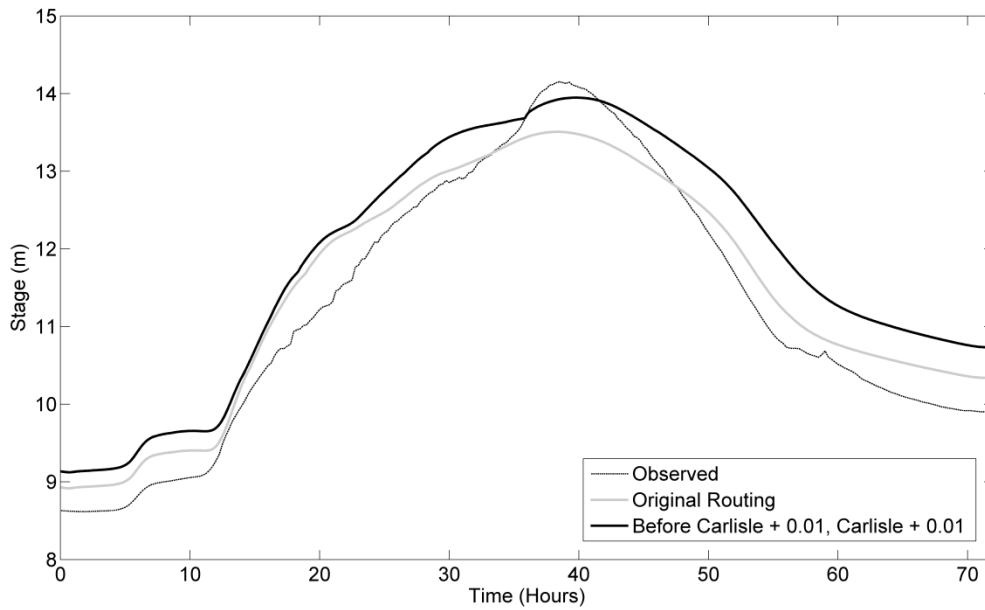
628 **Figure 2** Location map of the Eden Watershed. The red dots show the location  
 629 of the gauging stations used within this study)



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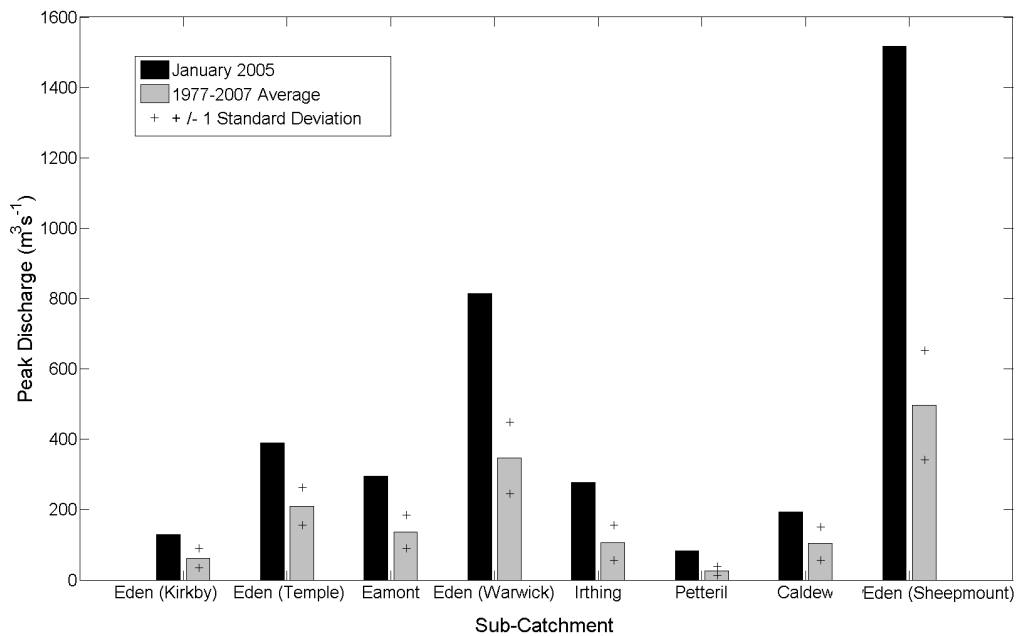
631 **Figure 3a** Sensitivity analysis of Sheepmount hydrograph to Manning's n.  
 632 Simulations represent changing Manning's n in different reaches of Eden. e.g. U/S  
 633 tribs (before -0.01, Carlisle +0.01 = Manning's n decreased by 0.01 before Carlisle  
 634 and increased by 0.01 in Carlisle itself.

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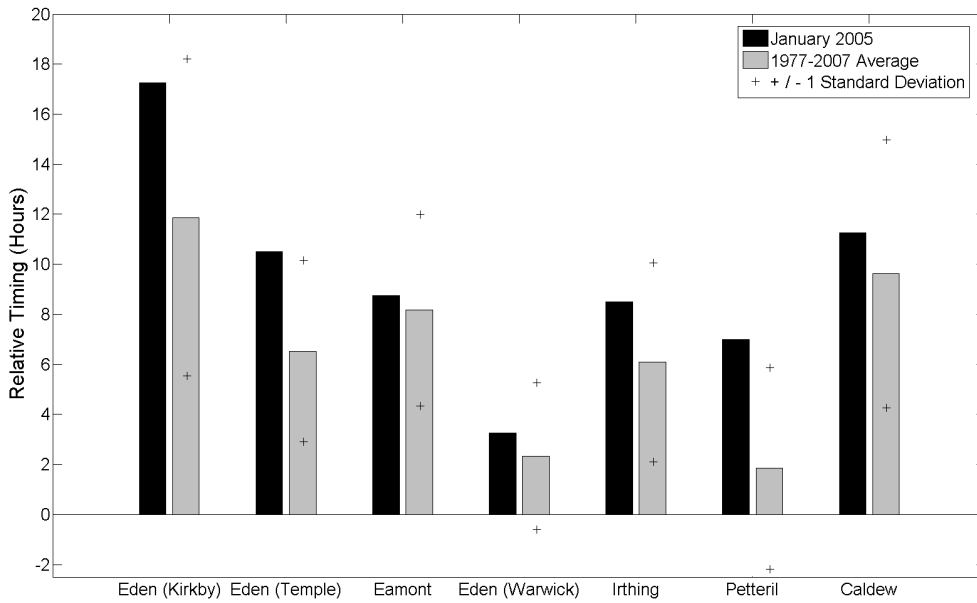
637 **Figure 3b** Calibration of Eden iSIS model using downstream gauging station of  
 638 Sheepmount in Carlisle to optimise for flood peak. (Performance statistics - Nash  
 639 Sutcliffe Coefficient = 0.85, RMSE = 0.67m, % error peak stage = -1.45%, % error in  
 640 volume = 5.2%)



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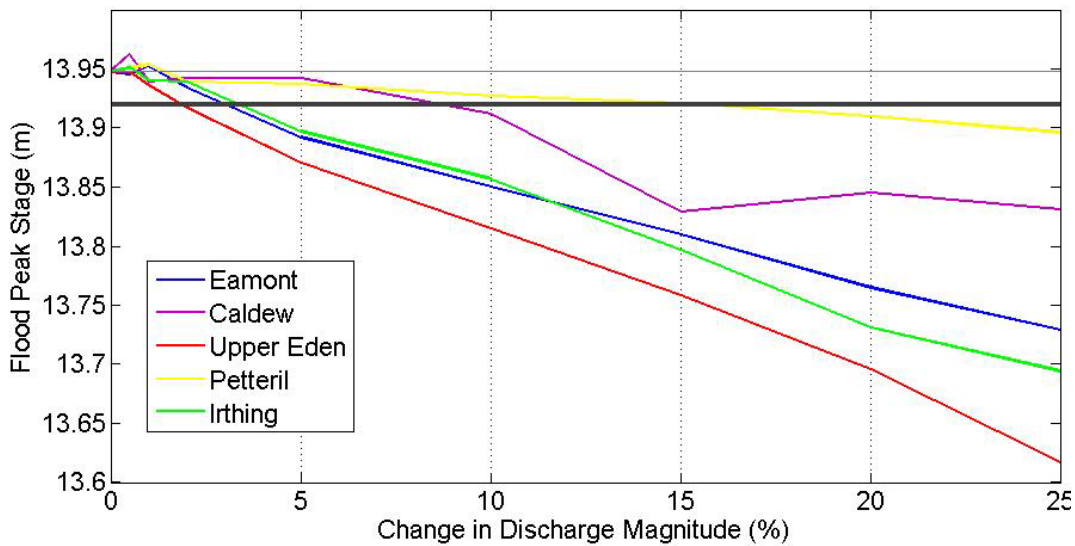
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643 **Figure 4a** Comparison of the January 2005 flood with the long term average in  
 644 terms of peak magnitudes from each sub-watershed.



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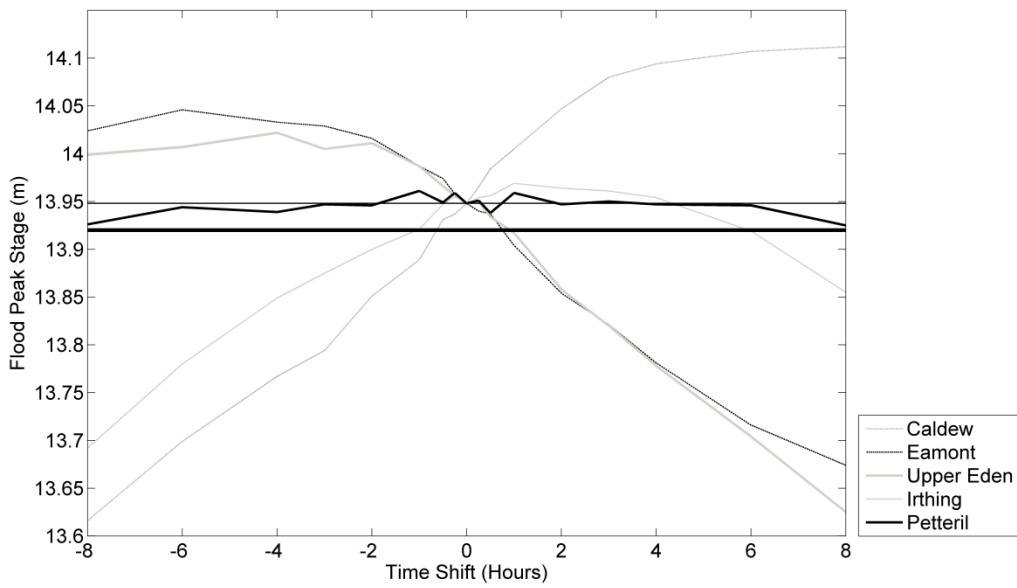
647 **Figure 4b** Comparison of the January 2005 flood with the long term average in  
 648 terms of the peak flow relative timing from each sub-watershed with respect to  
 649 Carlisle. A value of 0 means that both the tributary and the downstream main river  
 650 peak at the same time.



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652 **Figure 5** Sensitivity of peak stage at Carlisle (Sheepmount) to percentage  
 653 decreases in sub-watershed hydrograph contributions.

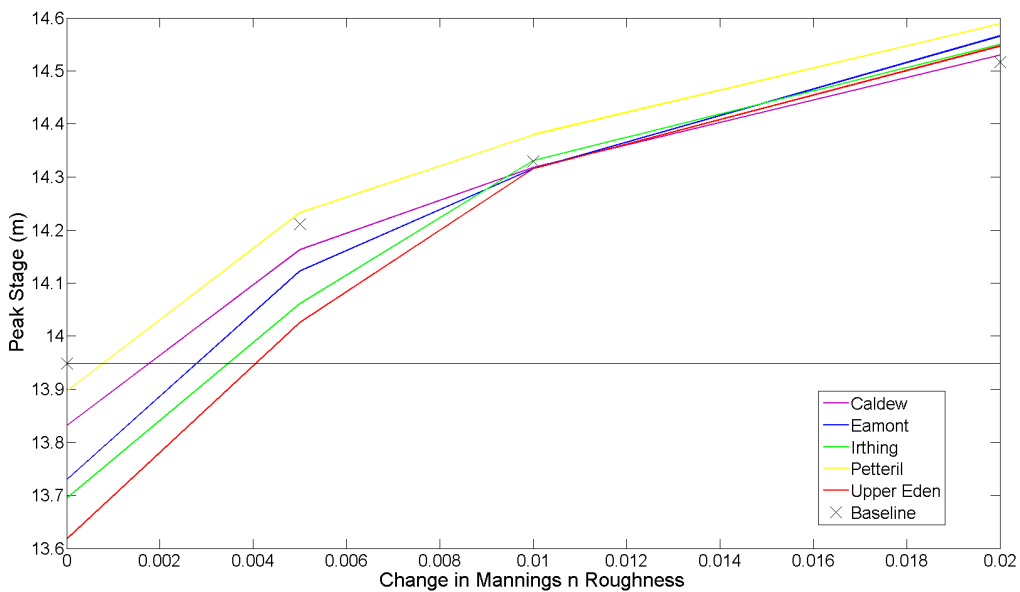




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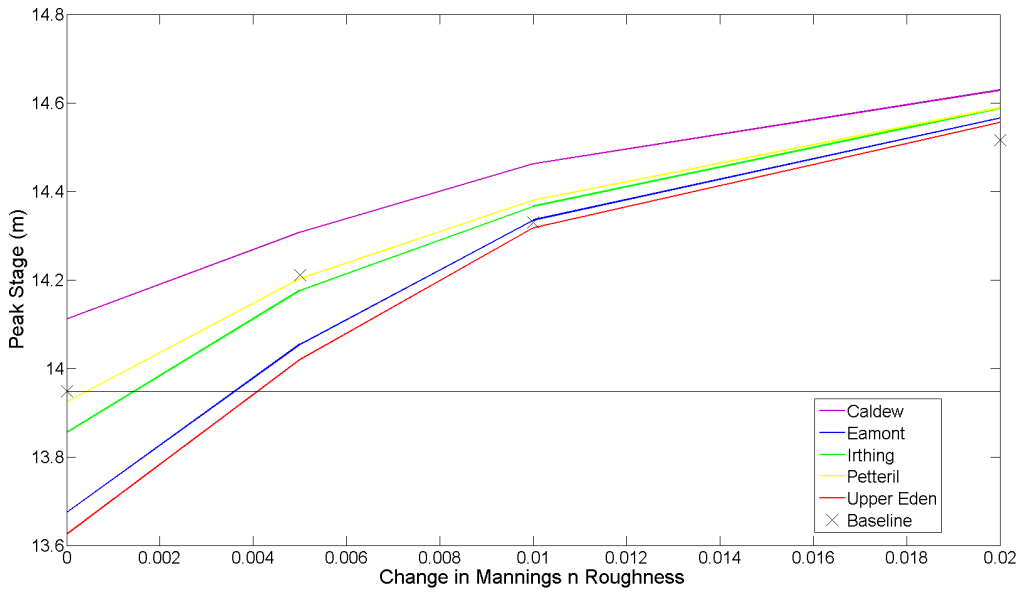
655 **Figure 6** Sensitivity of peak stage at Carlisle (Sheepmount) to timing shifts of the  
 656 contributing sub-watershed's hydrograph - light grey line = original peak flow, dark  
 657 grey line = bank full.

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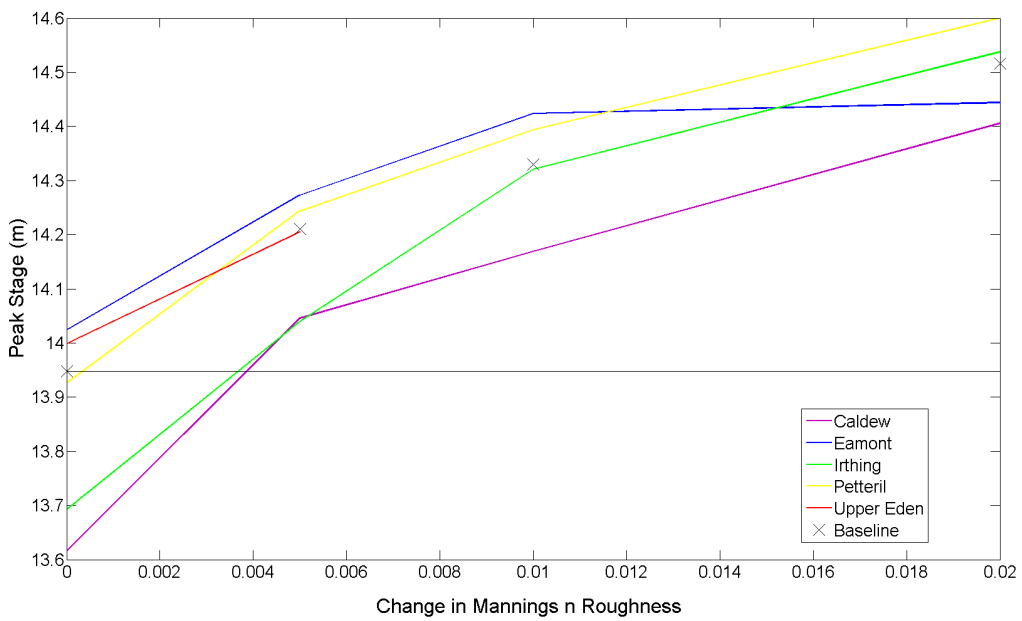
660 **Figure 7a** Uncertainty analysis of tributary 25% magnitude reduction scenario and  
 661 Mannings n.



662

663 **Figure 7a** Uncertainty analysis of tributary 8 hour delay scenario and Mannings n.

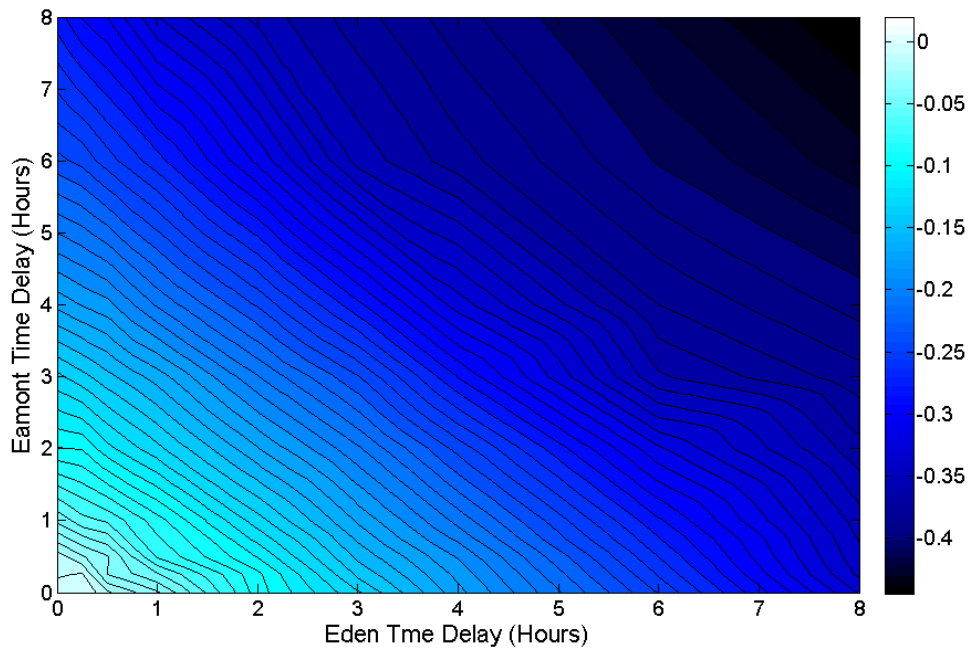
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666 **Figure 7c** Uncertainty analysis of tributary 8 hour earlier time scenario and Mannings n.

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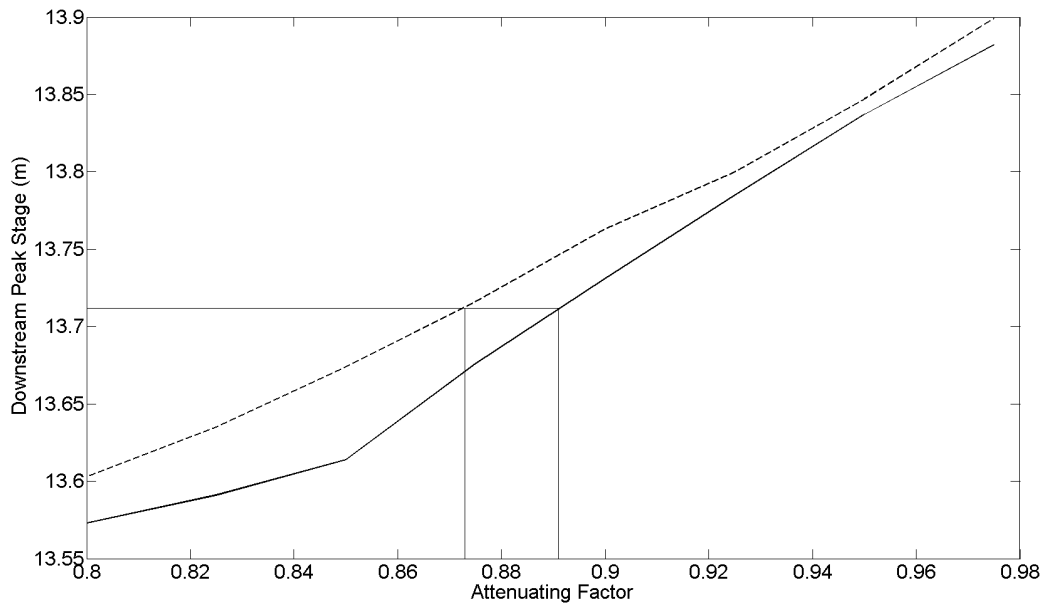


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669 **Figure 8** Sensitivity of peak stage at Sheepmount to timing shifts from multiple  
 670 sub-watersheds

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674 **Figure 9** Impact of varying degrees of attenuation of peak stage at Sheepmount.  
 675 Dashed line for Upper Eden, Solid line for Eamont. Attenuating factors for bankfull  
 676 stage are marked.

677

Tributary celerity	Distance (km)	Mean Wave Celerity km h <sup>-1</sup>	January 2005 Celerity (km h <sup>-1</sup> )	% Difference
Upper Eden (Kirkby Stephen) to Carlisle	100.2	9.90	5.81	-41.3%
Upper Eden (Temple Sowerby) to Carlisle	61.9	10.18	5.90	-42.0%
Eamont to Carlisle	59.8	11.81	6.83	-42.2%
Main Eden (Warwick Bridge) to Carlisle	17.2	5.96	5.29	-11.2%
Irthing to Carlisle	17.3	2.80	1.33	-52.5%
Petteril to Carlisle	6.4	1.54	0.91	-40.9%
Caldew to Carlisle	5.7	0.86	0.51	-40.7%

679 **Table 1** Celerity of flood wave as calculated from the travel time between the flood  
680 peak at each station and Carlisle and the associated distance.

681

682

683

Timing \ Magnitude	0 hrs	0.25 hr	0.50 hr	1 hrs	2 hrs	4 hrs	8 hrs
0%	0	0.002	-0.014	-0.031	-0.09	-0.17	-0.323
2%	-0.031	<b>-0.044</b> (-0.029)	<b>-0.053</b> (-0.045)	<b>-0.069</b> (-0.062)	-0.114 (-0.121)	-0.193 (-0.201)	-0.339 (-0.354)
5%	-0.077	<b>-0.085</b> (-0.075)	<b>-0.092</b> (-0.091)	-0.106 (-0.108)	-0.143 (-0.167)	-0.218 (-0.247)	-0.349 (-0.400)
10%	-0.133	<b>-0.141</b> (-0.131)	<b>-0.148</b> (-0.147)	<b>-0.167</b> (-0.164)	-0.198 (-0.223)	-0.274 (-0.303)	-0.367 (-0.456)
25%	-0.331	<b>-0.332</b> (-0.329)	-0.335 (-0.345)	-0.34 (-0.362)	-0.352 (-0.421)	-0.377 (-0.501)	-0.419 (-0.654)

684 **Table 2** Effect of both timing delays and magnitude reductions of the Upper  
685 Eden on the peak stage (metres) at Carlisle (Sheepmount). Top value is the  
686 simultaneous scenario, bottom value is the two separate scenario effects added  
687 together. (bold values indicate scenarios when the simultaneous scenario gives extra  
688 peak stage reduction than the two separate scenarios added together.)

689

Timing \ Magnitude	0 hrs	0.25 hr	0.50 hr	1 hr	2 hrs	4 hrs	8hrs
0%	0	-0.008	-0.011	-0.044	-0.094	-0.167	-0.274
2%	-0.014	<b>-0.028</b> (-0.022)	<b>-0.042</b> (-0.025)	<b>-0.066</b> (-0.058)	<b>-0.109</b> (-0.108)	<b>-0.181</b> (-0.181)	<b>-0.294</b> (-0.288)

<b>5%</b>	-0.056	-0.061 (-0.064)	<b>-0.075</b> (-0.067)	-0.091 (-0.100)	-0.126 (-0.150)	-0.196 (-0.223)	-0.316 (-0.330)
<b>10%</b>	-0.098	<b>-0.107</b> (-0.106)	<b>-0.112</b> (-0.109)	-0.13 (-0.142)	-0.165 (-0.192)	-0.233 (-0.265)	-0.341 (-0.372)
<b>25%</b>	-0.219	-0.229 (-0.227)	<b>-0.235</b> (-0.230)	-0.246 (-0.263)	-0.28 (-0.313)	-0.345 (-0.386)	-0.376 (-0.493)

690 **Table 3** *Effect of both timing delays and magnitude reductions of the Eamont*  
691 *on the peak stage at Carlisle (Sheepmount) (metres). Top value is the simultaneous*  
692 *scenario, bottom value is the two separate scenario effects added together. (bold*  
693 *values indicate scenarios when the simultaneous scenario gives extra peak stage*  
694 *reduction than the two separate scenarios added together.)*

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