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Overcoming the limitations of gold catalysts in hydrogenation: enhanced activity with full hydrogen utilization

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Abstract Application of nano-scale supported Au in catalytic hydrogenation delivers high chemoselectivity but low activity using (pressurized) H₂ far in excess of stoichiometric requirements. We have tackled the issues of low reaction rate and inefficient hydrogen utilization through a series of approaches taking Au/CeO₂ (mean Au size = 2.8 nm) as a test catalyst. Increased spillover hydrogen (using physical mixtures of Au/CeO₂ with CeO₂ and SiO₂) and the promotional effect of water (via catalytic dissociation on surface oxygen vacancies) resulted in a fourfold increase in the selective rate of furfural hydrogenation to furfuryl alcohol. In contrast, Pd/CeO₂ and Ni/CeO₂ promoted decarbonylation (to furan), hydrogenolysis (to 2-methylfuran) and ring reduction (to tetrahydrofurfuryl alcohol). Coupling (2-butanol → 2-butanone) dehydrogenation over Cu/SiO₂ (mean Cu size = 7.8 nm) with furfural hydrogenation over Au/CeO₂ further increased rate with full utilization of the hydrogen generated in dehydrogenation. The coupling strategy allows “hydrogen free” hydrogenation that circumvents the limitation of Au in standard catalytic hydrogenation. This can open new avenues to exploit the ultra-selectivity of Au for continuous production of high value commodity products.

Keywords Furfural hydrogenation · Au/CeO₂ · Hydrogen utilization · Coupled dehydrogenation/hydrogenation

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Introduction

The application of supported Au catalysts has focused on selective oxidation and environmental remediation in the conversion of volatile organics [1]. By comparison, use in hydrogenation, a key process across the chemical sector [2] is more limited [3]. Interest in Au catalysts for hydrogenation has been driven by the high chemoselectivity achieved in the reduction of polyfunctional molecules [4] but low reaction rate is a decided drawback [5]. Commercial hydrogenation processes are typically operated in excess (pressurized) H₂ in order to maximize product yield. Hydrogen is not a naturally occurring feedstock and production is fossil fuel based (by methane steam reforming and coal gasification [6]) where storage and transport represent serious constraints. A move away from reaction using compressed H₂ is a critical driver to achieve safer operations for large scale production. The use of a hydrogen carrier in transfer hydrogenation is a promising alternative that has been explored in organic synthesis using homogeneous [7] and heterogeneous catalysis [8, 9] in batch mode but it introduces additional catalyst/product separation and purification steps. Catalytic dehydrogenation of alcohols offers a possible in situ source of reactive hydrogen [10] as demonstrated by Nagaraja et al. [11] in coupling cyclohexanol dehydrogenation with furfural hydrogenation on Cr₂O₃ promoted Cu–MgO. However, the similarity (10 K difference) in the boiling points of the products necessitated difficult separation/purification while hydrogen utilization was poor (< 10%). 2-Butanone (used as solvent and in the production of plastics, coatings and films [12]) can be obtained from 2-butanol dehydrogenation with hydrogen release.

With the overarching goal of process sustainability, we have examined the hydrogenation of furfural as a biomass (corn cob and sugar cane bagasse) derived heterocyclic aldehyde [13]. Selective hydrogenation generates furfuryl alcohol, a high value chemical (130,000 tons per annum global production) used in the manufacture of resins/rubbers/adhesives and as a chemical building block for drug synthesis [14]. Gold on ceria has been shown to promote selective –C=O hydrogenation [15] and is used as a model catalyst in this work. Supported Pd and Ni with higher H₂ dissociative chemisorption capacity than Au [16] and enhanced activity in the hydrogenation of carbonyl compounds [17] were also tested to assess the performance of Au/CeO₂. Taking full H₂ utilization and increased selective hydrogenation rate as our ultimate objectives, we evaluate four approaches to increase the available surface reactive hydrogen: (i) modification of external H₂ partial pressure; (ii) enhanced spillover hydrogen associated with the support; (iii) hydrogen donation via catalytic water dissociation; (iv) coupling dehydrogenation with hydrogenation.

Experimental

Catalyst preparation

Ceria (Sigma-Aldrich, 99%) supported Au (0.7 mol%), Pd (0.8 mol%), Ni (0.5 mol%) and Cu/SiO₂ (15.2 mol%) were prepared by deposition–precipitation. In the synthesis of Au/CeO₂ an aqueous solution of urea (100-fold excess, Riedel-de Haën, 99%) with HAuCl₄ (2×10^{-3} mol dm⁻³, 400 cm³, Sigma-Aldrich, 99%) was mixed with the ceria support (10 g). The suspension was stirred (600 rpm) and heated (2 K min^{-1}) to 353 K in air where the pH progressively increased (to ca. 7) after 3 h as a result of urea decomposition. The solid was separated by filtration and washed with distilled water until Cl free (based on AgNO₃ test). In the synthesis of Pd/CeO₂ and Ni/CeO₂, an aqueous solution (2×10^{-3} mol dm⁻³, 300 cm³) of the metal precursor (Pd(NO₃)₂ or Ni(NO₃)₂, Sigma-Aldrich, 99%) was added to CeO₂ (10 g), Na₂CO₃ (2 mol dm⁻³, Riedel-de Haën, 99%) slowly added to the resultant suspension until pH > 10, heating (2 K min^{-1}) to 353 K for 4 h resulting in deposition of Pd(OH)₂ and NiCO₃ [18]. The filtered solid was washed with distilled water and dried in a vacuum oven at 333 K for 12 h. Silica supported Cu was prepared with NaOH (Riedel-de Haën, 99%) as precipitation agent where 20 g (fumed) silica powder (Sigma-Aldrich, 99%) were dispersed in a solution of Cu(NO₃)₂ (25×10^{-2} mol dm⁻³, 200 cm³, Sigma-Aldrich, 99%). The suspension was stirred (600 rpm) at room temperature for 1 h with the addition of aqueous NaOH (2 M) until pH > 10 and subsequent heating to 353 K maintained for 4 h to ensure homogeneous Cu(OH)₂ deposition [19]. The solid was separated by filtration, washed with distilled water until pH 7 and dried at 393 K overnight. The dried sample was calcined (in air) at 10 K min^{-1} to 723 K for 4 h to generate copper oxide (CuO) [19]. All the samples were sieved (ATM fine test sieves) to mean particle diameter = 75 μm. The samples were activated in 60 cm³ min⁻¹ H₂ to 523–723 K (at $2\text{--}10 \text{ K min}^{-1}$) with a final isothermal hold for 1–2 h and passivated at ambient temperature in 1% v/v O₂/He for ex situ characterization.

Catalyst characterization

Metal content was measured by atomic absorption spectroscopy using a Shimadzu AA-6650 spectrometer with an air-acetylene flame from the diluted extract in aqua regia (25% v/v HNO₃/HCl). Temperature programmed reduction (TPR), H₂ chemisorption (at 498 K) and subsequent temperature programmed desorption (TPD) were conducted on the CHEM-BET 3000 (Quantachrome) unit equipped with a thermal conductivity detector (TCD) for continuous monitoring of gas composition and the TPR WinTM software for data acquisition/manipulation. Samples were loaded into a U-shaped Pyrex glass cell (3.76 mm i.d.) and reduced in $17 \text{ cm}^3 \text{ min}^{-1}$ 5% v/v H₂/N₂ to 523–723 K (at $2\text{--}10 \text{ K min}^{-1}$) where the effluent gas passed through a liquid N₂ trap. The activated samples were swept with $65 \text{ cm}^3 \text{ min}^{-1}$ N₂ for 1.5 h, cooled to 498 K and subjected to H₂ chemisorption (BOC, 99.99%) using pulse (10–50 μl) titration. The hydrogen pulses were repeated

until the signal area was constant, indicating surface saturation. In blank tests, there was no measurable H_2 uptake on the supports. Samples were thoroughly flushed in N_2 ($65 \text{ cm}^3 \text{ min}^{-1}$) to remove weakly bound hydrogen and subjected to TPD (at 50 K min^{-1}) to 973 K with a final isothermal hold until the signal returned to baseline. Scanning transmission electron microscopy (STEM) was performed using a JEOL 2200FS field emission gun-equipped transmission electron microscope unit, employing Gatan Digital Micrograph 1.82 for data acquisition/manipulation. Samples for analysis were prepared by dispersion in acetone and deposited on a holey carbon/Cu grid (300 Mesh). Surface area weighted mean metal particle size (d) was determined from a count of up to 600 particles according to:

$$d = \frac{\sum_i n_i d_i^3}{\sum_i n_i d_i^2} \quad (1)$$

Here n_i is the number of particles of diameter d_i .

Catalytic procedure

Reactions (independent hydrogenation of furfural (in H_2) and coupled dehydrogenation/hydrogenation of 2-butanol/furfural) were carried out at atmospheric pressure and 498 K in situ after activation in a continuous flow fixed-bed tubular reactor ($i.d. = 15 \text{ mm}$). Reaction conditions ensured negligible internal/external mass and heat transfer limitations. A layer of borosilicate glass beads served as preheating zone where the reactant was vaporized and reached reaction temperature before contacting the catalyst bed. Isothermal conditions ($\pm 1 \text{ K}$) were maintained by diluting the catalyst with ground glass ($75 \mu\text{m}$); reaction temperature was continuously monitored by a thermocouple inserted in a thermowell within the catalyst bed. The reactant(s) was(were) delivered to the reactor via a glass/Teflon air-tight syringe and Teflon line using a microprocessor controlled infusion pump (Model 100 kd Scientific). The independent hydrogenation of furfural was tested in a co-current flow of H_2 with furfural ($GHSV = 5 \times 10^3 \text{ h}^{-1}$ and molar metal to furfural feed rate (n/F) = $5 \times 10^{-3} \text{ h}$). Coupled dehydrogenation/hydrogenation was conducted in N_2 ($GHSV = 3 \times 10^3 \text{ h}^{-1}$, $n_{Au}/F = 5 \times 10^{-3}$ – $11 \times 10^{-3} \text{ h}$, molar Cu/Au = 65–150). The reactor effluent was analyzed by capillary GC (Perkin-Elmer Auto System XL gas chromatograph equipped with a programmed split/splitless injector and a flame ionization detector, employing a DB-1 ($50 \text{ m} \times 0.33 \text{ mm } i.d.$, $0.20 \mu\text{m}$ film thickness) capillary column (J&W Scientific)). In control experiments, passage of each reactant in a stream of H_2 or N_2 through the empty reactor or over the support alone did not result in any detectable conversion. Reactant (i) fractional conversion (X) is defined by:

$$X_i = \frac{[reactant]_{i,in} - [reactant]_{i,out}}{[reactant]_{i,in}} \quad (2)$$

The selectivity (S) to product (j) is given by:

$$S_j(\%) = \frac{[product]_{j,out}}{[reactant]_{i,in} - [reactant]_{i,out}} \times 100 \quad (3)$$

Here the subscripts “in” and “out” refer to the inlet and outlet gas streams, respectively. Repeated reactions using different samples from the same batch of catalyst delivered raw data reproducibility and mass balance within $\pm 5\%$. Catalytic activity is quantified in terms of initial conversion/hydrogenation rate obtained from time on-stream measurements [20].

Results and discussion

The TPR of Au/CeO₂ (Fig. 1aI) exhibits a single positive peak (H₂ consumption, $T_{max} = 418$ K), which can be ascribed to Au³⁺ → Au⁰ reduction and is in line with published data ($T_{max} = 375$ –500 K) for ceria supported Au involving a range of syntheses [21]. Hydrogen consumption during TPR (12 mol_{H₂} mol_{Au}⁻¹) was eight times greater than that required for reduction to metallic gold, indicative of partial support reduction with the formation of surface oxygen vacancies [22]. STEM analysis (Fig. 1bI) revealed pseudo-spherical metal particles at the nano-scale (1–5 nm, Fig. 1cI) with an associated surface area weighted mean of 2.8 nm. It has been noted elsewhere [23] that Au particle size < 10 nm is critical for significant hydrogenation activity. Hydrogen chemisorption on Au/CeO₂ was appreciably lower than that measured under reaction conditions for the benchmark Pd/CeO₂ and Ni/CeO₂ (Table 1). This is due to the filled 3*d* band in Au that results in a high energy barrier for dissociative adsorption and low H–Au binding strength [24].

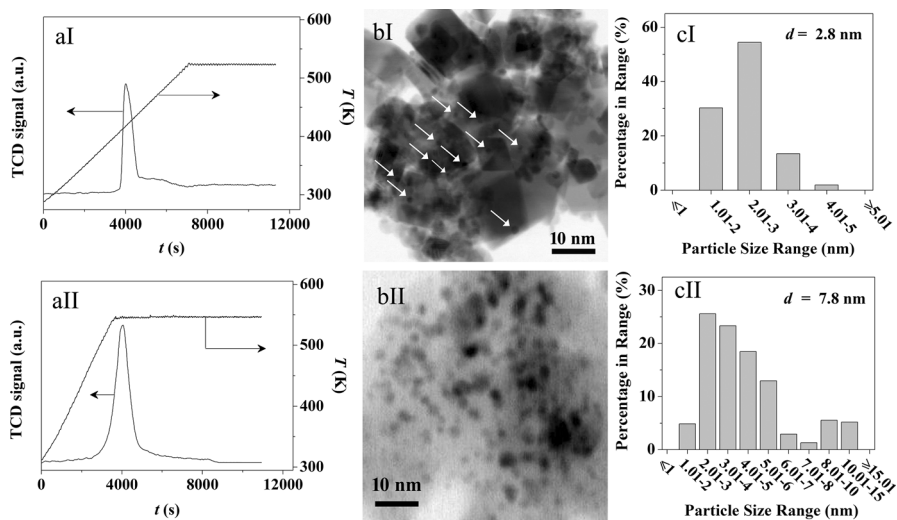


Fig. 1 a TPR profile, b representative STEM image (arrows identify Au nanoparticles) with c associated metal particle size distribution histogram for **I** Au/CeO₂ and **II** Cu/SiO₂

Table 1 Physicochemical properties and catalytic response in furfural hydrogenation over CeO₂ supported Au, Pd and Ni

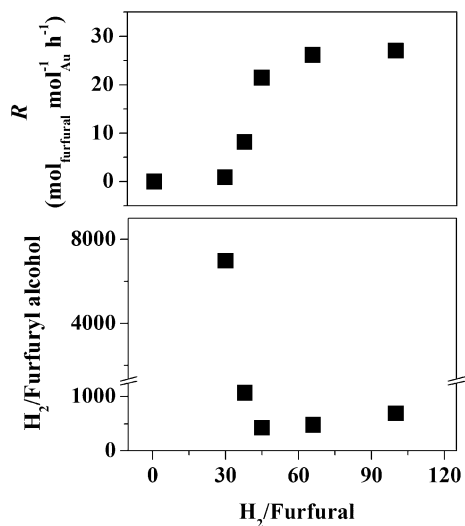
Supported metal	Loading (mol%)	<i>d</i> (nm)	H ₂ chemisorption at 498 K (μmol g ⁻¹)	Rate (mol _{furfural} mol _{metal} ⁻¹ h ⁻¹)	Selectivity (%) FA/2-MF/ F/THF
Au	0.7	2.8	2	26	100/0/0/0
Pd	0.8	3.7	62	47	0/58/24/18
Ni	0.5	2.0	22	8	0/19/73/8

Reaction conditions *T* = 498 K, *P* = 1 atm

FA furfuryl alcohol, *2-MF* 2-methylfuran, *F* furan, *THF* tetrahydrofurfuryl alcohol

Given that H₂ activation is a limiting factor, we explored the effect of increasing inlet H₂/furfural on reaction rate (Fig. 2). In every case, reaction over Au/CeO₂ was fully selective to the target furfuryl alcohol, an important result in the light of reported batch liquid phase furfural hydrogenation over Au/SiO₂ where conversion was negligible even at high H₂ pressure (1.0 MPa) [25]. We observed no detectable catalytic activity at the reaction stoichiometry (H₂/furfural = 1) but rate increased to reach an upper value (26 mol_{furfural} mol_{Au}⁻¹ h⁻¹) at H₂/furfural > 60 (Fig. 2). Hydrogen utilization efficiency (represented by inlet H₂ to outlet furfuryl alcohol ratio) was enhanced with increasing inlet H₂/furfural (to 45, Fig. 2). The restricted capacity of Au for H₂ adsorption/dissociation resulted in an upper limit in terms of rate with measurably lower efficiencies at higher H₂/furfural (> 45). Hydrogen utilization is a critical consideration in terms of process sustainability where the best result (H₂/furfuryl alcohol = 420) is far removed from the target stoichiometry (= 1). We evaluated Pd/CeO₂ and Ni/CeO₂ to assess the catalytic

Fig. 2 Furfural hydrogenation rate (*R*) and H₂ utilization (H₂/furfuryl alcohol) as a function of inlet H₂/furfural over Au/CeO₂. Reaction conditions *T* = 498 K, *P* = 1 atm, *n*_{Au}/*F* = 5 × 10⁻³ h

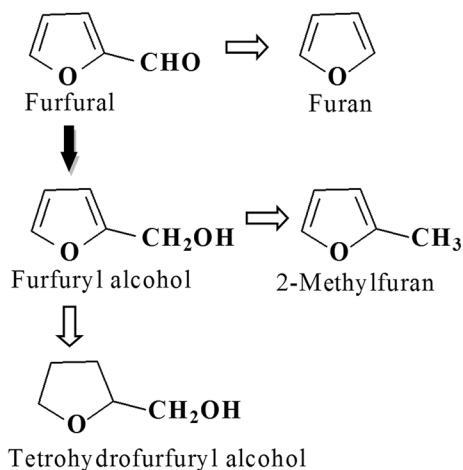


performance of Au/CeO₂ and the results are presented in Table 1. There was no detectable furfuryl alcohol formation over either catalyst. Pd/CeO₂ with the greatest H₂ uptake capacity (Table 1) delivered the highest rate but promoted secondary decarbonylation to furan, hydrogenolysis of furfuryl alcohol to 2-methylfuran and ring reduction to tetrahydrofurfuryl alcohol (Fig. 3). Furan was the main product formed over Ni/CeO₂. Sitthisa and Resasco [26] recorded decarbonylation (to furan) over Pd/SiO₂ and ring opening (to butanal, butanol and butane) over Ni/SiO₂ in the gas phase hydrogenation of furfural. Our results demonstrate a dependence of product distribution on the catalytic metal where Au facilitates exclusive reduction of the carbonyl group to the target alcohol.

Hydrogen dissociated on metal sites “spills” across the metal/support interface onto the support surface and even across solid/solid grain boundaries (e.g. catalyst + support physical mixtures) [27]. This spillover hydrogen contributes to hydrogenation activity [28]. Spillover has been reported for supported Au catalysts following hydrogen treatment at 423–673 K and can be quantified by TPD [29]. The TPD profile for Au/CeO₂ (Fig. 4) is characterized by H₂ release (180 μmol g⁻¹, $T_{max} = 788$ K) that far exceeded H₂ chemisorption (Table 1) and can be attributed to spillover desorption [28]. The incorporation of CeO₂ or SiO₂ in a physical mixture with Au/CeO₂ resulted in measurably greater H₂ desorption (Fig. 4). A consequent increase in furfural hydrogenation rate (from 26 to 31 mol_{furfural} mol_{Au}⁻¹ h⁻¹) was obtained while retaining full selectivity to furfuryl alcohol and confirms contribution from spillover hydrogen to increase selective hydrogenation rate.

Water is an environmentally benign solvent that can act as hydrogen donor in water gas shift and steam reforming over (CeO₂ and Fe₂O₃) supported Au [30, 31]. The effect of incorporating water in the furfural feed was tested for reaction over Au/CeO₂ (Fig. 5) where a threefold higher rate was achieved at H₂O/furfural = 0.2–1. We envision a surface mechanism (schematic in Fig. 5) where spillover hydrogen results in the formation of oxygen vacancies (steps I–II).

Fig. 3 Reaction pathways for the hydrogenation of furfural over CeO₂ supported Au (solid arrow) and Pd and Ni (open arrows)



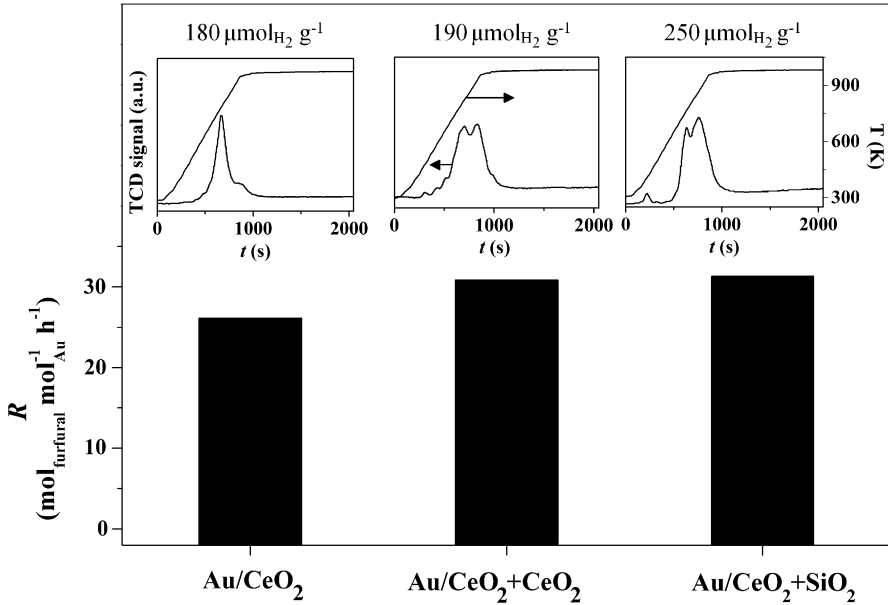


Fig. 4 Furfural hydrogenation rate (R) and H_2 TPD profiles (as insets) for Au/CeO_2 and physical mixtures of Au/CeO_2 with CeO_2 and SiO_2 . Reaction conditions $T = 498 \text{ K}$, $P = 1 \text{ atm}$, $n_{\text{Au}}/F = 5 \times 10^{-3} \text{ h}$, $\text{H}_2/\text{furfural} = 66$

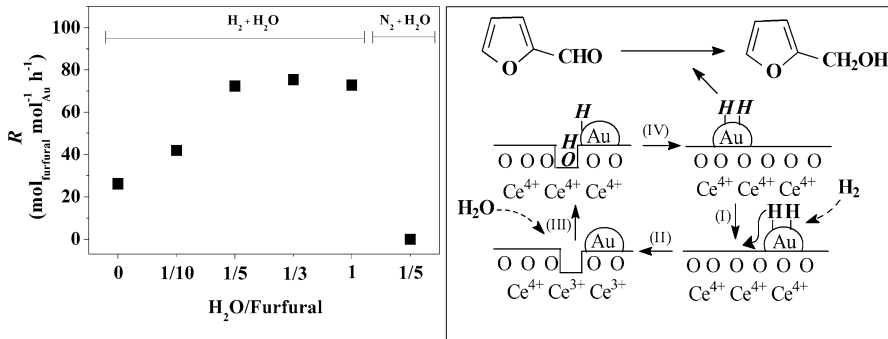


Fig. 5 Furfural hydrogenation rate (R) as a function of inlet $\text{H}_2\text{O}/\text{furfural}$ molar ratio with proposed reaction mechanism (steps I–IV) illustrating the effect of water addition on furfural hydrogenation (to furfuryl alcohol). Reaction conditions $T = 498 \text{ K}$, $P = 1 \text{ atm}$, $n_{\text{Au}}/F = 5 \times 10^{-3} \text{ h}$, $\text{H}_2/\text{furfural} = 66$

Dissociative interaction of H_2O generates OH that is consumed in a re-oxidation of the support (step III) with the generation of reactive protons (step IV) that attack the furfural carbonyl group to produce the alcohol. At $\text{H}_2\text{O}/\text{furfural} = 0.2$, a switch from H_2 to N_2 in the feed did not result in any detectable conversion (Fig. 5). This suggests an activated process that involves continuous creation, consumption and regeneration of oxygen vacancies, requiring a co-current $\text{H}_2/\text{H}_2\text{O}$ inlet with hydroxyl consumption and release of reactive hydrogen for $-\text{C}=\text{O}$ reduction.

Viable commercial application requires more efficient hydrogen utilization. Coupling 2-butanol dehydrogenation with furfural hydrogenation generates two high value products (2-butanone and furfuryl alcohol) that can be readily separated (100 K difference in boiling points at 1 atm) by standard distillation [32]. Au/CeO₂ exhibited negligible activity in the dehydrogenation of 2-butanol and there is a requirement for an alternative (dehydrogenation) catalytic metal. Copper is effective in dehydrogenation [33] and Cu/SiO₂ was chosen as a suitable candidate to work in tandem with Au/CeO₂. TPR of Cu/SiO₂ (Fig. 1aII) resulted in H₂ consumption (1 mol_{H₂} mol_{Cu}⁻¹) that matched the requirement for the Cu²⁺ → Cu⁰ reduction step. This is consistent with the work of Smith et al. who demonstrated formation of zero valent Cu at *T* > 523 K [34]. The activated catalyst exhibited Cu particles in the 1–15 nm range with a surface area weighted mean of 7.8 nm (Fig. 1bII, cII). Dehydrogenation of 2-butanol over Cu/SiO₂ generated 2-butanone as sole product at a rate (42 mol_{furfural} mol_{Cu}⁻¹ h⁻¹) that was greater than hydrogenation over Au/CeO₂, guaranteeing sufficient hydrogen in the coupled reaction (Fig. 6a). Under the same reaction conditions, Cu/SiO₂ delivered negligible activity (< 2 mol_{furfural} mol_{Cu}⁻¹ h⁻¹) in furfural conversion and consequently does not contribute significantly to hydrogenation in the coupled reaction (Fig. 6a). We evaluated catalytic coupling (in N₂) over a physical mixture of Au/CeO₂ + Cu/SiO₂ with varying Cu/Au ratio and the results are presented in Fig. 6b. In every case, 2-butanone and furfuryl alcohol were the only products obtained. Rate increased (from 26 to 85 mol_{furfural} mol_{Au}⁻¹ h⁻¹) with decreasing Cu/Au (from 150 to 65). Our results demonstrate successful utilization by Au/CeO₂ of the hydrogen generated in situ by Cu/SiO₂. Dehydrogenation proceeds via a two-step H abstraction mechanism [35]. This supply of reactive hydrogen circumvents the limitations associated with hydrogen activation/dissociation by Au and delivers an improved furfural hydrogenation rate. Activity in the coupled system was not affected by water addition unlike the stand alone furfural hydrogenation. This can be attributed to insufficient

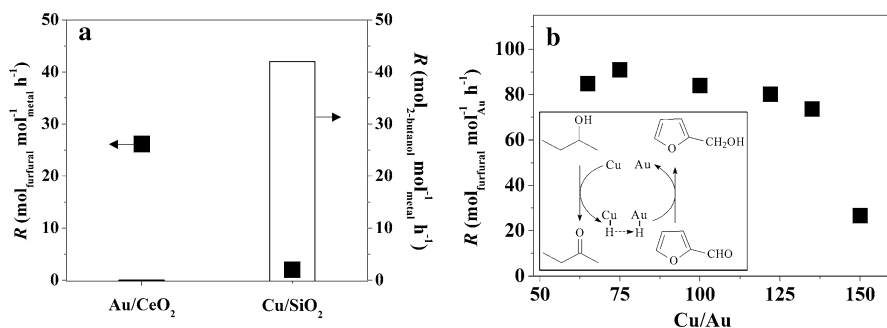


Fig. 6 **a** Reaction rate in stand-alone furfural hydrogenation (R , filled square) and dehydrogenation of 2-butanol (R , bars) over Au/CeO₂ and Cu/SiO₂; **b** furfural hydrogenation rate (R) as a function of Cu/Au molar ratio in coupled 2-butanol dehydrogenation with furfural hydrogenation. *Inset* schematic representation of mechanism involved in coupling of 2-butanol dehydrogenation over Cu with furfural hydrogenation over Au. *Reaction conditions* $T = 498$ K, $P = 1$ atm, 2-BuOH/furfural = 15

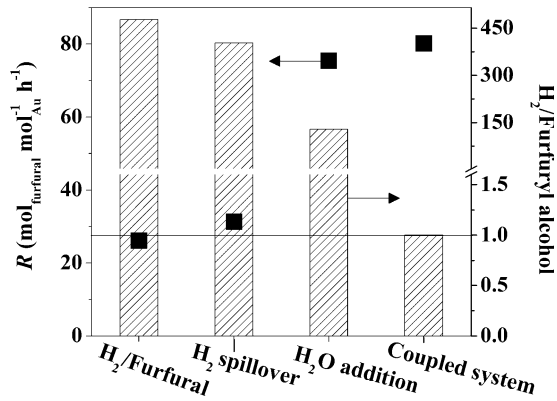


Fig. 7 Comparison of catalytic response for different hydrogen supply strategies: furfural hydrogenation rate (R ; filled square) and H₂ utilization (H₂/furfuryl alcohol, bars) over Au/CeO₂ as a result of variation in inlet H₂/furfural, increased spillover H₂, promotion by water dissociation and coupling with dehydrogenation. *Note* horizontal line represents full H₂ utilization under stoichiometric conditions. *Reaction conditions* $T = 498$ K, $P = 1$ atm

hydrogen availability for ceria reduction to form the oxygen vacancies necessary for water dissociation and release of reactive hydrogen (see Fig. 5).

The different approaches we have considered in this work to enhance hydrogen utilization and selective furfural hydrogenation rate over supported Au are summarized in Fig. 7. The use of a conventional compressed H₂ source suffers from low utilization efficiency (H₂/furfuryl alcohol = 420) and the reaction is conducted in excess H₂. Incorporation of oxides (CeO₂ or SiO₂) in a physical mixture with Au/CeO₂ and inclusion of water in the feed generate reactive hydrogen via spillover and water dissociation, respectively. This resulted in a fourfold increase in rate but hydrogen utilization was still far removed from stoichiometric requirements. The dehydrogenation/hydrogenation coupling strategy enabled full utilization of (in situ generated) hydrogen via dehydrogenation where H₂/furfuryl alcohol converged at reaction stoichiometry. This approach delivers improved process efficiency and offers clear advantages over standard hydrogenation applications with new opportunities for exploitation of the chemoselectivity exhibited by supported Au catalysts.

Conclusions

We have demonstrated that Au/CeO₂ (Au mean size = 2.8 nm) promotes continuous gas phase hydrogenation of furfural to furfuryl alcohol. Under the same reaction conditions, Pd/CeO₂ and Ni/CeO₂ promoted decarbonylation, hydrogenolysis and furan ring reduction. An increase in available surface hydrogen on Au/CeO₂ via (i) increased H₂ content in the feed, (ii) spillover hydrogen and (iii) catalytic water dissociation resulted in an increase in selective hydrogenation rate. Full hydrogen utilization and higher alcohol production rate was achieved by

coupling catalytic dehydrogenation (2-butanol \rightarrow 2-butanone) over Cu/SiO₂ (mean Cu size = 7.8 nm) with furfural hydrogenation over Au/CeO₂. This circumvents use of external pressurized H₂ with the production of two high value products that are readily separated by distillation. Our results demonstrate a feasible solution to the limitations of Au in reductive processes and can open new directions in “hydrogen free” hydrogenation.

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