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Continuous Gas Phase Catalytic Transformation of Levulinic Acid to -Valerolactone over Supported Au Catalysts

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2 **Continuous Gas Phase**

3 **Catalytic Transformation of**

4 **Levulinic Acid to γ -Valerolactone over**

5 **Supported Au Catalysts**

6

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1 **ABSTRACT**

2 **BACKGROUND:** γ -Valerolactone (GVL) is a high value chemical obtained from
3 hydrogenation of bio-derived levulinic acid (LA). Work to date has focused on batch
4 pressurised catalytic systems where high GVL yield is challenging. In this work, we examine
5 the role of support redox and acidity properties in the continuous gas phase hydrogenation of
6 aqueous LA at ambient pressure over gold on Al₂O₃, CeO₂ and TiO₂; Pd/Al₂O₃ served as a
7 benchmark in catalyst tests.

8 **RESULTS:** We achieved 100% GVL yield under stoichiometric conditions (inlet H₂/LA = 1)
9 over supported Au (mean size = 3.0-4.3 nm). Greater catalytic activity was recorded for Au
10 on reducible TiO₂ and CeO₂. Under the same reaction conditions, Pd/Al₂O₃ delivered higher
11 LA consumption rates but promoted formation of pentanoic acid.

12 **CONCLUSIONS:** GVL formation proceeds *via* 4-hydroxypentanoic as reactive
13 intermediate. Surface oxygen vacancies (confirmed by O₂ titration) formed during
14 temperature programmed reduction of reducible oxides activate LA for reaction. Greater
15 GVL productivity (with full hydrogen utilisation) is demonstrated in this work relative to
16 state-of-the art supported Pd and Ru catalysts.

17

18 **Keywords:** Selective hydrogenation; levulinic acid; γ -valerolactone; Au catalysts; support
19 effects.

20

1 SYMBOLS

LA	Levulinic acid
GVL	γ -Valerolactone
HPA	Hydroxypentanoic acid
AGL	α -Angelica lactone
i.d.	Internal diameter, mm
d	Metal nanoparticle mean size, nm
TPR	Temperature programmed reduction
TPD	Temperature programmed desorption
TCD	Thermal conductivity detector
SSA	Specific surface area, $\text{m}^2 \text{g}^{-1}$
STEM	Scanning transmission electron microscopy
T_{max}	Temperature maximum in catalyst activation by TPR, K
P	Pressure, atm
T	Reaction temperature, K
L_{bed}	Catalyst bed length, mm
V_{bed}	Catalyst bed volume, mm^3
n	Moles of metal in the catalyst bed, mol
F	Levulinic acid feed rate, mol h^{-1}
$GHSV$	Gas hourly space velocity, h^{-1}
FID	Flame ionisation detector
X	Fractional conversion
S_j	Selectivity to product "j", %
k	Kinetic rate constant, h^{-1}

1 INTRODUCTION

2 γ -Valerolactone (GVL) is a lignocellulose building block chemical used as an
3 intermediate in alkane (jet fuel, gasoline and diesel fuel), aromatic (fuel additives), polymer
4 and solvent production.¹ The main route to GVL is the hydrogenation of levulinic acid (LA),
5 obtained from cellulose, starch, or C6 sugars² *via* low cost (\$0.09-0.22 kg⁻¹) acid
6 hydrolysis.^{3,4} The reaction pathways from a compilation of the literature⁵⁻⁷ on
7 LA \rightarrow GVL transformation are presented in **Figure 1**. GVL production proceeds *via*
8 hydrogenation and dehydration steps. The predominant pathway is still a matter of debate
9 where variations in operating conditions,⁵ choice of support⁸ and metal⁹ or solvent¹⁰ impacts
10 on catalytic activity and/or selectivity.

11 The catalytic hydrogenation of LA using both homogeneous¹¹ and heterogeneous⁵
12 systems has been investigated. Heterogeneous catalysis offers advantages in terms of product
13 separation and catalyst reuse. Work to date has largely dealt with pressurised (5-250 bar)
14 batch liquid phase conversion in organic solvents (1,4-dioxane, methanol and toluene) where
15 full selectivity to GVL at high conversions remains challenging.¹¹⁻¹⁴ Continuous GVL
16 formation at ambient pressure facilitates higher throughput. In catalytic hydrogenation,
17 control over contact time can govern conversion¹⁵ and selectivity.¹⁶ Reviews by Wright and
18 Palkovits in 2012,⁵ Yan *et al.* in 2015⁷ and Delidovich *et al.* in 2016¹⁷ identified supported Pd
19 and Ru as the best catalysts for continuous gas phase transformation of LA with a
20 productivity of 81-91 mmol_{GVL} g_{metal}⁻¹ h⁻¹ and 90-98.6% GVL yield. Use of toxic 1,4-
21 dioxane¹⁸ as solvent and excess hydrogen are process sustainability issues to be addressed.

22 The use of supported gold catalysts for the transformation of biomass-derived
23 feedstock to value-added chemicals is showing promise.¹⁹ Notable examples include
24 aldehyde reduction (*e.g.* 2-hydroxymethyl-5-furfural \rightarrow 2,5-bis(hydroxymethyl)furan)²⁰,

1 dehydration of carbohydrates²¹ and hydrogenation/dehydration of succinic anhydride to γ -
2 butyrolactone²². Lewis and Brønsted acid sites contribute to catalytic dehydration²³ (**Figure**
3 **1**, steps **(I)**, **(IV)**, **(VII)**, and **(VIII)**). In the case of reducible oxide supports (*e.g.* titania and
4 ceria), oxygen vacancies generated by the loss of structural oxygen from the oxide sub-
5 lattice²⁴ can modify reactant adsorption/activation and influence catalytic performance²⁵.
6 These vacancies can fix oxygen in water,²⁶ alcohols²⁷ and aldehydes²⁸. Increased rate and
7 carbonyl reduction selectivity in the conversion of aldehydes has been ascribed to facilitated
8 -C=O activation at oxygen deficient sites in CeO₂²⁹ and Fe₂O₃³⁰. Using DFT calculations,
9 Baker *et al.*³¹ identified oxygen vacancies in Pd/TiO₂ as the catalytically active sites for -C=O
10 reduction in furfural hydrogenation. The opposite effect is also possible where strong binding
11 of oxygenated reactants to these vacancies³² has been deemed responsible for lower
12 hydrogenation activity.³³

13 In this work, we evaluate the impact of the support redox (reducibility) and acid
14 properties in the continuous hydrogenation of LA over a series of oxide (Al₂O₃, CeO₂ and
15 TiO₂) supported Au catalysts, taking Pd/Al₂O₃ as a benchmark. We examine the reaction
16 pathways and consider the effect of varying inlet H₂/LA, using water as a solvent with a view
17 to clean production of GVL.

18 **EXPERIMENTAL**

20 **Catalyst Preparation and Activation**

21 The oxide carriers (γ -Al₂O₃ (Puralox, Condea Vista Co.), CeO₂ (Grace Davison) and
22 TiO₂ (P25, Degussa)) were used as received. Supported (1.0-3.0% wt.) Au catalysts were
23 prepared by deposition-precipitation. Urea (100-fold excess, Riedel-de Haën, 99%), used as
24 basification agent, was added to an aqueous solution of HAuCl₄ ($4 \times 10^{-5} - 5 \times 10^{-3}$ M; 20–50
25 cm³, Sigma-Aldrich, 99%) containing the support (5-30 g). The suspension was stirred and

1 heated to 353 K (2 K min⁻¹) for 3 h in a He purge where the pH progressively increased to *ca.*
2 7 after 3 h as a result of thermally induced urea decomposition with Au³⁺ deposition.³⁴ The
3 resultant solid was separated by centrifugation, washed with deionised water until the wash
4 water was Cl-free (AgNO₃ test) and dried in He (45 cm³ min⁻¹) at 373 K (2 K min⁻¹) for 5 h.
5 A commercial Pd/Al₂O₃ (1.2% wt. Pd, Sigma-Aldrich) catalyst was employed as benchmark.
6 Prior to use, the catalysts were sieved to 75 µm average particle diameter (ATM fine test
7 sieves) and activated in 60 cm³ min⁻¹ H₂ at 2 K min⁻¹ to 573–603 K. Samples were passivated
8 in 1% v/v O₂/He at ambient temperature for *ex situ* analysis.

9 10 ***Catalyst Characterisation***

11 The (Au and Pd) metal content was measured by atomic absorption spectroscopy
12 (Shimadzu AA-6650 spectrometer with an air-acetylene flame) from the diluted extract in
13 aqua regia (25% v/v HNO₃/HCl). Temperature programmed reduction (TPR), H₂/O₂/NH₃
14 chemisorption, temperature programmed desorption (TPD) and specific surface area (SSA)
15 measurements were recorded using the commercial CHEM-BET 3000 (Quantachrome
16 Instruments) unit equipped with a thermal conductivity detector (TCD) for monitoring gas
17 composition and the TPR WinTM software for data acquisition/manipulation. Samples (0.05-
18 0.1 g) were loaded into a U-shaped Quartz cell (3.76 mm i.d.), outgassed for 30 min and total
19 SSA recorded in a 30% v/v N₂/He flow with undiluted N₂ (BOC, 99.9%) as internal standard.
20 Two cycles of N₂ adsorption-desorption were employed using the standard single point BET
21 method. TPR analysis was conducted in 17 cm³ min⁻¹ (Brooks mass flow controller) 5% v/v
22 H₂/N₂ at 2 K min⁻¹ to 573–603 K where the effluent gas passed through a liquid N₂ trap.
23 Samples were maintained at the final isothermal hold in a flow of H₂/N₂ until the signal
24 returned to baseline, swept with 65 cm³ min⁻¹ N₂ for 1.5 h, cooled to reaction (493 K, H₂
25 chemisorption) or ambient (NH₃ chemisorption) temperature and subjected to pulse (10-1000

1 μl) titration (BOC, $\geq 99.98\%$). Hydrogen/ammonia pulses were repeated until the signal area
2 was constant and there was no detectable uptake. Ammonia TPD was conducted to determine
3 total acidity.³⁵ Samples were thoroughly flushed in N_2 ($65 \text{ cm}^3 \text{ min}^{-1}$) for 1.5 h post- NH_3
4 titration to remove weakly bound NH_3 and heated at 30 K min^{-1} (in $65 \text{ cm}^3 \text{ min}^{-1} \text{ N}_2$) to 973
5 K. Oxygen chemisorption was performed to assess the extent of support reduction,³⁶ where
6 the samples were swept with $65 \text{ cm}^3 \text{ min}^{-1} \text{ He}$ for 1.5 h post-TPR, cooled to 493 K and
7 subjected to O_2 pulse ($10 \mu\text{l}$) titration. It has been demonstrated elsewhere that Au
8 contribution to total O_2 adsorbed is negligible.³⁷ SSA and gas uptake values were
9 reproducible to $\pm 5\%$. Gold and Pd metal particle morphology (size and shape) was
10 determined by scanning transmission electron microscopy (STEM) using a JEOL 2200FS
11 operated at an accelerating voltage of 200 kV, employing Gatan Digital Micrograph 1.82 for
12 data acquisition/manipulation. Samples for analysis were prepared by dispersion in acetone
13 and deposited on a holey Cu grid (300 mesh). The number weighted mean Au and Pd
14 diameters (d) were determined from a count of up to 800 particles.³⁸

15 *Gas Phase Hydrogenation of Levulinic acid (LA)*

17 *Materials*

18 LA (98%) and GVL (99%) were supplied by Sigma-Aldrich and used as received. All
19 the gases (H_2 , N_2 , O_2 and He) were of ultra-high purity (BOC, $\geq 99.99\%$).

20 *Catalytic System*

22 Reactions were performed at ambient pressure over the temperature range 493-573 K,
23 immediately after *in situ* catalyst activation in a fixed bed vertical continuous plug-flow glass
24 reactor (i.d. = 12 mm). A layer of borosilicate glass balls (2 mm diameter; height = 3 cm)
25 served as preheating zone, ensuring the reactant was vaporised and reached reaction

1 temperature before contacting the catalyst. Isothermal conditions (± 1 K) were maintained by
2 diluting the catalyst bed ($L_{\text{bed}} = 2$ mm; $V_{\text{bed}} = 226$ mm³; fraction of catalyst in the bed by
3 volume = 0.1-1) with ground glass (75 μm). Reaction temperature was continuously
4 monitored by a thermocouple inserted in a thermowell within the catalyst bed. An aqueous or
5 organic (toluene) solution of LA (0.29 M) was delivered to the reactor *via* a glass/teflon air-
6 tight syringe and a teflon line at a fixed calibrated flow rate using a microprocessor controlled
7 infusion pump (Model 100, KD Scientific). A co-current flow of LA and H₂, N₂ or H₂+N₂
8 was maintained at $GHSV = 2 \times 10^4$ h⁻¹ where inlet H₂/LA was varied from stoichiometry (=1
9 for GVL formation) to far in excess (=420); gas flow rate was monitored using a Humonics
10 (Model 520) digital flowmeter. The molar metal (n) to inlet LA feed rate (F) spanned the
11 range $5 \times 10^{-4} - 1 \times 10^{-2}$ h. In a series of blank tests, reactions using GVL or LA as reactant in
12 a stream of H₂ through the empty reactor or over the support alone did not result in any
13 detectable conversion.

14 Analytical Method and Activity/Selectivity Evaluation

16 The reactor effluent was frozen in a liquid nitrogen trap and analysed by capillary GC
17 (Perkin-Elmer Auto System XL gas chromatograph equipped with a programmed
18 split/splitless injector and flame ionisation detector (FID)) using a Stabilwax (fused silica) 30
19 m \times 0.32 mm i.d., 0.25 μm film thickness capillary column (RESTEK), employing Turbo-
20 Chrom Workstation Version 6.3.2 (for Windows) for data storage and manipulation. Product
21 composition was based on detailed calibration plots (not shown) using commercial samples.
22 Catalytic activity is quantified in terms of fractional conversion (X)

$$23 \quad X = \frac{LA_{\text{in}} - LA_{\text{out}}}{LA_{\text{in}}} \quad (1)$$

24 extracted from time on-stream measurements.³⁹ Selectivity in terms of the target GVL (S_{GVL})

1 is given by

$$2 \quad S_{\text{GVL}} = \frac{\text{GVL}_{\text{out}}}{\text{LA}_{\text{in}} - \text{LA}_{\text{out}}} \times 100 \quad (2)$$

3 where the subscripts "in" and "out" refer to the inlet and outlet streams. Repeated reactions
4 with different samples from the same batch of catalyst delivered conversion/selectivity values
5 reproducible to within $\pm 5\%$; carbon mass balance was complete to better than $\pm 9\%$.

6 7 **RESULTS AND DISCUSSION**

8 *Catalyst Characterisation*

9 Catalyst physico-chemical characteristics are given in **Table 1**. The SSA range from 52
10 $\text{m}^2 \text{g}^{-1}$ (Au/TiO₂) to 166 $\text{m}^2 \text{g}^{-1}$ (Au/Al₂O₃) and the values obtained for each system are in
11 agreement with those reported in the literature.^{40,41} The TPR profiles of laboratory
12 synthesised Au/Al₂O₃ (**A**), Au/CeO₂ (**B**) and Au/TiO₂ (**C**) are presented in **Figure 2(I)** with
13 associated H₂ consumption in **Table 1**. Activation of Pd/Al₂O₃ by TPR followed the
14 procedure described previously.⁴² Au/Al₂O₃ exhibited a single positive peak at 461 K that is
15 comparable with the literature.⁴³ Hydrogen consumption matched the requirements for Au³⁺
16 \rightarrow Au⁰. A lower temperature reduction peak was in evidence for Au/CeO₂ ($T_{\text{max}} = 420$ K) and
17 Au/TiO₂ ($T_{\text{max}} = 376$ K) and can be linked to weaker Au-support interactions⁴⁰ resulting in a
18 more facile reduction of the metal phase⁴⁴. Hydrogen consumption during TPR of Au/CeO₂
19 ($5 \times 10^2 \mu\text{mol g}^{-1}$) and Au/TiO₂ ($2 \times 10^2 \mu\text{mol g}^{-1}$) exceeded the amount required for
20 reduction of the metal precursor (**Table 1**), indicative of partial support reduction.⁴⁵
21 Hydrogen chemisorption on all the Au catalysts was lower than the benchmark Pd/Al₂O₃
22 (**Table 1**), which can be explained by the higher activation barrier for dissociative H₂
23 adsorption on Au.⁴⁶ The consensus from the literature suggests that H₂ adsorption on Au is
24 dependent on temperature and Au coordination.⁴⁷ Smaller Au particles exhibit a greater

1 preponderance of corner and edge sites that facilitate H₂ adsorption, which is favoured by a
2 higher titration temperature.⁴⁸ Dissociated H₂ chemisorbed on Au can spill onto the support
3 and promote superficial reduction of the oxide carrier with the generation of oxygen
4 vacancies, an effect that has been reported for Au/CeO₂⁴⁹ and Au/TiO₂⁵⁰.

5 Oxygen chemisorption post-TPR was negligible on Au/Al₂O₃ and Pd/Al₂O₃ (**Table 1**),
6 consistent with the *non*-reducibility of Al₂O₃ where temperatures ≥ 1373 K are required for
7 oxide reduction.⁵¹ Greater uptake on Au/CeO₂ and Au/TiO₂ is consistent with vacancy
8 formation during TPR of these reducible oxides. Representative STEM images (**I**) and
9 associated particle size distribution histograms (**II**) for Au/Al₂O₃ (**A**), Au/CeO₂ (**B**) and
10 Au/TiO₂ (**C**) are provided in **Figure 3**. The Au particles are in the 1-8 nm size range, which
11 has been identified as crucial for hydrogenation activity.⁵² Au/CeO₂ and Au/TiO₂ showed a
12 narrower distribution of smaller metal particles, which can be linked to stabilisation at
13 oxygen vacancies that serves to inhibit sintering during TPR.⁵³ The Pd/Al₂O₃ sample
14 exhibited similar mean metal size (**Table 1**) and is a suitable reference catalyst to assess the
15 catalytic performance of supported Au in LA hydrogenation.

16 Surface acidity was determined by NH₃ chemisorption/TPD. Total acidity measurements
17 coincided for titration and TPD; the desorption profiles for Au/Al₂O₃ (**A**), Au/CeO₂ (**B**) and
18 Au/TiO₂ (**C**) are provided in **Figure 2(II)**. The three catalysts exhibited a principal desorption
19 peak for NH₃ release over the 600-973 K range, characteristic of strong acid sites, *i.e.* NH₃
20 desorption at $T \geq 673$ K.^{8,54} Surface acidity in the case of Al₂O₃, CeO₂ and TiO₂ is associated
21 with uptake at Al³⁺, Ce⁴⁺ or Ti⁴⁺ Lewis acid centres, as demonstrated by XPS,⁵⁵ temperature-
22 programmed reaction,⁵⁵ NMR⁵⁶ and FT-IR^{57,58} measurements. The quantity of NH₃
23 chemisorbed/desorbed (**Table 1**) on the three Au catalysts ($12\text{-}28 \times 10^{-2}$ mmol g⁻¹) was
24 comparable with that reported for Al₂O₃,^{40,41} CeO₂,⁵⁹ and TiO₂^{60,61} supported Au systems (10-

1 $38 \times 10^{-2} \text{ mmol g}^{-1}$.

2

3 ***Catalyst Performance***

4 Reaction over supported Au under conditions of excess hydrogen ($\text{H}_2/\text{LA} = 420$)
5 generated GVL as sole product at $X \leq 0.75$ (**Figure 4(I)**). This response finds agreement with
6 the work of Du *et al.*⁶² in batch liquid phase conversion of LA + formic acid (5 bar) over
7 (ZrO_2 , TiO_2 , SiO_2) supported Au where CO_2 was formed as by-product (from formic acid).
8 We provide here the first reported catalytic data for gas phase continuous flow operation at
9 ambient pressure over Au catalysts. Taking the reaction pathways presented in **Figure 1**,
10 GVL generation through the formation of (levulinic and hydroxy levulinic) esters (steps **(I-**
11 **II)**) is associated with batch liquid operation with alcohol solvents.⁶³ The $\text{LA} \rightarrow \text{GVL}$
12 composite hydrogenation/dehydration is possible *via* two routes. Reaction through steps **(VI)**
13 and **(VII)** involves hydrogenation of the ketone group at metal sites to form 4-
14 hydroxypentanoic acid (HPA) that undergoes acid-catalysed ring closure (intramolecular
15 esterification).⁶ There is theoretical (DFT)^{64,65} and experimental⁶⁵ evidence that $\text{LA} \rightarrow \text{HPA}$
16 hydrogenation (step **(VI)**) is rate-determining. HPA is highly reactive and readily undergoes
17 dehydration to GVL.⁶⁶ Alternatively, dehydration of LA (step **(VIII)**) on acid sites generates
18 α -angelica lactone (AGL) that undergoes reduction to GVL (step **(IX)**).⁶⁷ The HPA or AGL
19 intermediates were not isolated in the product mixture. Conversion of LA to AGL *via* step
20 **(VIII)** is favoured by replacing H_2 with N_2 as gas carrier, circumventing reduction (step
21 **(VI)**). Switching from H_2O to toluene as LA solvent should also favour dehydration to AGL.
22 Reaction (at 573 K) in N_2 using toluene over the three Au catalysts resulted in exclusive LA
23 \rightarrow AGL at a similar low conversion ($X \leq 0.08$). At the same reaction temperature, catalyst
24 tests using the three systems in H_2 with H_2O promoted $\text{LA} \rightarrow \text{GVL}$ at 10-fold higher
25 conversion. Transformation of an aqueous LA feed (in H_2) to GVL must proceed

1 predominantly *via* HPA in a sequential hydrogenation and dehydration (steps **(VI)** and **(VII)**).
2 It is established that acid sites contribute to dehydration.²³ The three Au catalysts exhibit
3 similar surface acidity (see **Figure 2(II)** and **Table 1**), which did not promote significant LA
4 → AGL but must contribute to HPA → GVL (step **(VII)**) in the sequential conversion of LA.
5 Balla *et al.*⁶⁸ and Kumar and co-workers⁶⁹ showed that catalytic activity in the gas phase
6 transformation of LA → AGL is dependent on the concentration⁶⁸ and type⁶⁹ of acid sites.

7 We have previously established the applicability of pseudo-first order kinetics for
8 hydrogenation over Au under plug-flow conditions where H₂ was maintained in excess⁴⁷
9 according to

$$10 \quad \ln(1 - X)^{-1} = k \times \left(\frac{n}{F} \right) \quad (3)$$

11 where the parameter n/F has the physical significance of contact time. The rate constants (k)
12 obtained from linear regression of $\ln(1 - X)^{-1}$ vs. n/F (**Figure 5**) were fitted to an Arrhenius
13 expression to give an apparent activation energy for LA → GVL of 35 kJ mol⁻¹ (see inset to
14 **Figure 5** for Au/Al₂O₃). This is within the range (26-54 kJ mol⁻¹)⁶ reported for liquid phase
15 reaction over Ru catalysts. The activity of Au/Al₂O₃ was appreciably lower than that of Au on
16 reducible supports (**Table 1**). Differences in rate can result from variations in H₂ uptake under
17 reaction conditions.⁷⁰ However, the three supported catalysts exhibit an equivalent
18 chemisorption capacity (**Table 1**). It is significant that Au/CeO₂ and Au/TiO₂ with similar
19 density of oxygen vacancies (and greater than Au/Al₂O₃) delivered an equivalent catalytic
20 activity. A possible contribution due to LA adsorption/activation at these vacancies should
21 then be considered. Calaza *et al.*⁷¹ have established (by TPD, RAIRS and DFT) carbonyl
22 group activation at oxygen vacancies on CeO₂. To probe this effect we evaluated the catalytic
23 response of physical mixtures of Au/Al₂O₃ with (non-reducible) Al₂O₃ and (reducible)

1 TiO₂/CeO₂. Reaction over Au/Al₂O₃+Al₂O₃ and Au/Al₂O₃ delivered the same LA
2 consumption rate (300 mmol_{GVL} g_{metal}⁻¹ h⁻¹). In contrast, Au/Al₂O₃+TiO₂ and Au/Al₂O₃+CeO₂
3 combinations exhibited measurably higher rates (500-600 mmol_{GVL} g_{metal}⁻¹ h⁻¹). Oxygen
4 vacancy formation in CeO₂ and TiO₂ as part of the Au/Al₂O₃+TiO₂ and Au/Al₂O₃+CeO₂
5 mixtures is possible by spillover hydrogen migration across solid/solid grain boundaries.⁷²
6 The greater activity of Au/Al₂O₃ with reducible CeO₂ and TiO₂ suggests a direct contribution
7 of these surface defects to catalytic activity. A similar conclusion was reached by Manyar *et*
8 *al.*⁷³ and Hu and co-workers⁷⁴ in the hydrogenation of carboxylic acids and dimethyl
9 succinate (to γ -butyrolactone) over TiO₂ supported Pt and Mn spinel-supported Cu,
10 respectively. At higher LA conversion ($X > 0.75$), GVL selectivity declined (**Figure 4(I)**) due
11 to the formation of pentanoic acid. The generation of pentanoic acid can result from HPA
12 hydrogenation-dehydration (step **(IV)** in **Figure 1**) or further conversion of GVL (step **(V)**).
13 Kumar *et al.*⁶⁹ has shown by combined pyridine adsorption/DRIFTS analysis and kinetic
14 measurements that acid sites promote GVL ring opening to pentanoic acid. Using GVL as
15 reactant under the same reaction conditions, we recorded negligible conversion ($X < 0.03$),
16 suggesting step **(IV)** as the predominant source of pentanoic acid.

17 Unwanted transformation of HPA to pentanoic acid (*via* step **(IV)** in **Figure 1**)
18 requires hydrogen. With a view to maximise GVL formation and limit pentanoic acid
19 formation we evaluated the catalytic response to modifications in H₂ content in the feed (inlet
20 H₂/LA); the results obtained are presented in **Figure 4(II)**. A decrease in H₂/LA served to
21 increase GVL selectivity to reach 100% yield over the three catalysts under stoichiometric
22 conditions. Levulinic acid transformation is typically operated under an excess of pressurised
23 gaseous H₂ in order to maximise product yield.¹¹⁻¹³ Mohan *et al.*⁷⁵ studied the effect of H₂/LA
24 molar ratio for reaction over Ni/H-ZSM-5 and reported a maximum 92% GVL yield at H₂/LA

1 = 8. The authors recorded lower conversions at $H_2/LA < 8$ while formation of pentanoic acid
2 was promoted at $H_2/LA > 8$. To the best of our knowledge, this is the first report of 100%
3 GVL yield in continuous operation with full hydrogen utilisation. Under these reaction
4 conditions, Pd/Al₂O₃ delivered a higher LA consumption rate than Au/Al₂O₃ (1090 vs. 300
5 mmol_{GVL} g_{metal}⁻¹ h⁻¹), that correlates well with the reported higher activity for Pd (vs. Au) in
6 hydrogenations^{76,77} but promoted undesired pentanoic acid ($S_{\text{Pentanoic acid}} = 10\%$). We have
7 recorded 100% yield of GVL with an order of magnitude greater productivity relative to the
8 state-of-the art supported Pd and Ru catalysts^{5,7,17}. Our results demonstrate that oxide
9 supported Au promotes GVL formation *via* HPA where catalytic activity is sensitive to the
10 redox nature of the oxide carrier.

11 12 **CONCLUSIONS**

13 In the gas phase continuous catalytic conversion of (aqueous) LA, 100% yield of
14 target GVL was achieved under stoichiometric conditions ($H_2/LA = 1$) over oxide (Al₂O₃,
15 CeO₂ and TiO₂) supported Au. The formation of GVL results from
16 hydrogenation/dehydration with HPA as reactive intermediate. Oxygen titration following
17 TPR established partial reduction of CeO₂ and TiO₂ where Au on reducible supports
18 delivered a higher GVL production rate (relative to Au/Al₂O₃) that is linked to LA activation
19 at surface oxygen vacancies. Palladium on Al₂O₃ as benchmark exhibited higher LA
20 consumption rates but promoted formation of pentanoic acid. Higher H₂ feed content (H_2/LA
21 >2) generated pentanoic acid over the Au catalysts. Continuous GVL formation at ambient
22 pressure from an aqueous LA feed represents a significant advancement over current
23 pressurised batch liquid operations using organic solvents. We have demonstrated full
24 hydrogen utilisation and an order of magnitude higher GVL production rate than current
25 state-of-the art supported Pd and Ru catalysts.

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Table 1. Physico-chemical characteristics of supported Au and Pd catalysts and pseudo-first order rate constant for the transformation of levulinic acid to γ -valerolactone at 493 K (k_{493}).

Catalyst	Au/Al ₂ O ₃	Au/CeO ₂	Au/TiO ₂	Pd/Al ₂ O ₃
SSA (m ² g ⁻¹)	166	108	52	156
TPR H ₂ consumption $\times 10^2$ ($\mu\text{mol g}^{-1}$)	1 ^a /1 ^b	5 ^a /2 ^b	2 ^a /1 ^b	-
H ₂ chemisorption ($\mu\text{mol g}^{-1}$) ^c	5	3	4	17
O ₂ chemisorption $\times 10^{-2}$ ($\mu\text{mol m}^{-2}$) ^c	1	21	23	2
d (nm)	4.3	3.0	3.2	3.0
(NH ₃ chemisorption ^d / TPD) $\times 10^{-2}$ (mmol g ⁻¹)	15/16	23/28	12/12	-
k_{493} (h ⁻¹)	33	83	96	128

^aexperimentally determined value

^btheoretical value for Au³⁺→Au⁰

^ctitration at 493K

^dtitration at 298K

Figure Captions

Figure 1: Reaction pathways involved in the transformation of levulinic acid (LA) to the target (framed) γ -valerolactone (GVL).

Figure 2: (I) TPR and (II) NH_3 -TPD profiles for (A) Au/ Al_2O_3 , (B) Au/ CeO_2 and (C) Au/ TiO_2 .

Figure 3: Representative (I) STEM images and (II) associated Au particle size distributions for (A) Au/ Al_2O_3 , (B) Au/ CeO_2 and (C) Au/ TiO_2 .

Figure 4: Variation of γ -valerolactone selectivity (S_{GVL}) with (I) levulinic acid (LA) fractional conversion (X) under reaction conditions in excess of hydrogen ($\text{H}_2/\text{LA} = 420$) and (II) inlet H_2/LA at full LA conversion ($X = 1$) over Au/ Al_2O_3 (\circ), Au/ CeO_2 (\triangle) and Au/ TiO_2 (\diamond); *Reaction Conditions:* $T = 493\text{-}573$ K, $P = 1$ atm, $n/F = 5 \times 10^{-4} - 1 \times 10^{-2}$ h.

Figure 5: (I) Pseudo-first order kinetic plot for the conversion of levulinic acid (LA) to γ -valerolactone (GVL) over Au/ Al_2O_3 (\circ), Au/ CeO_2 (\triangle) and Au/ TiO_2 (\diamond) with (II) Arrhenius plot for reaction over Au/ Al_2O_3 ; *Reaction Conditions:* $T = 493\text{-}573$ K, $P = 1$ atm, $\text{H}_2/\text{LA} = 420$.

Figure 1

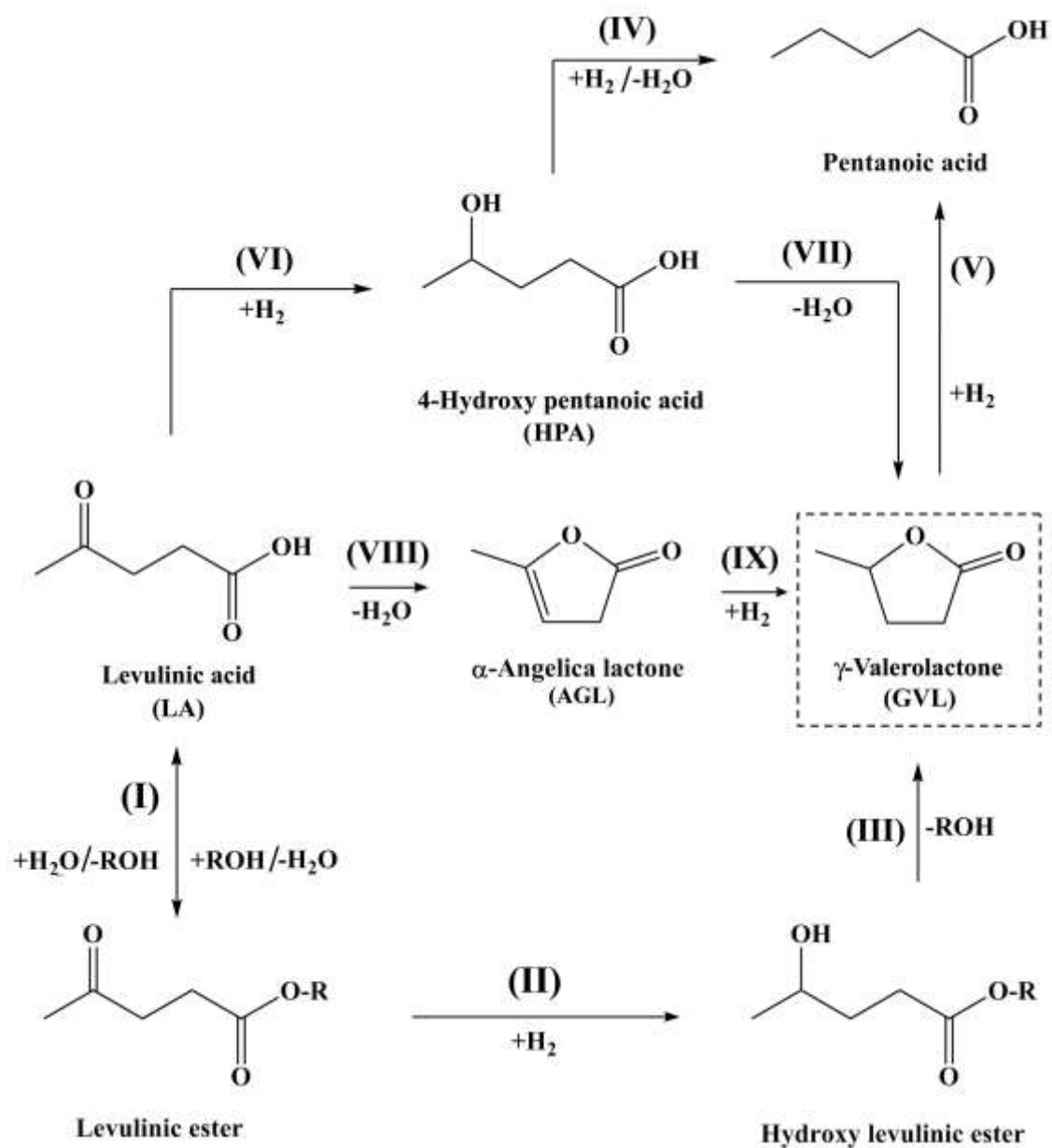


Figure 2

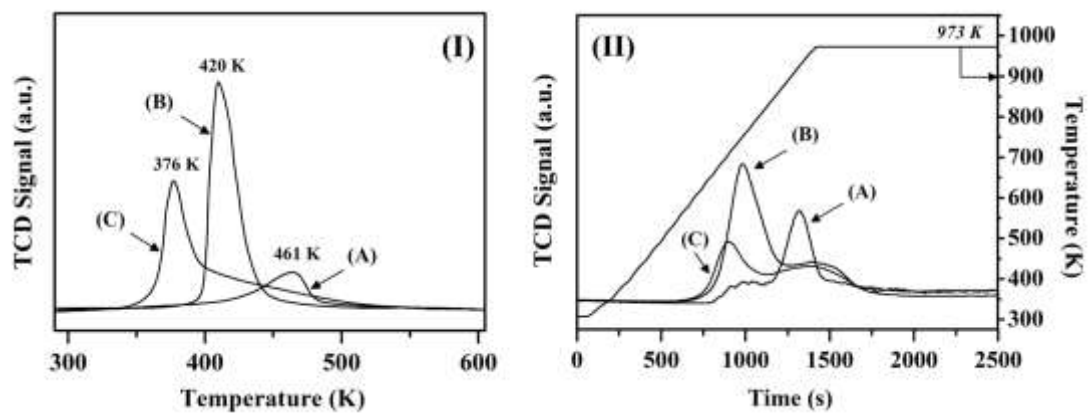


Figure 3

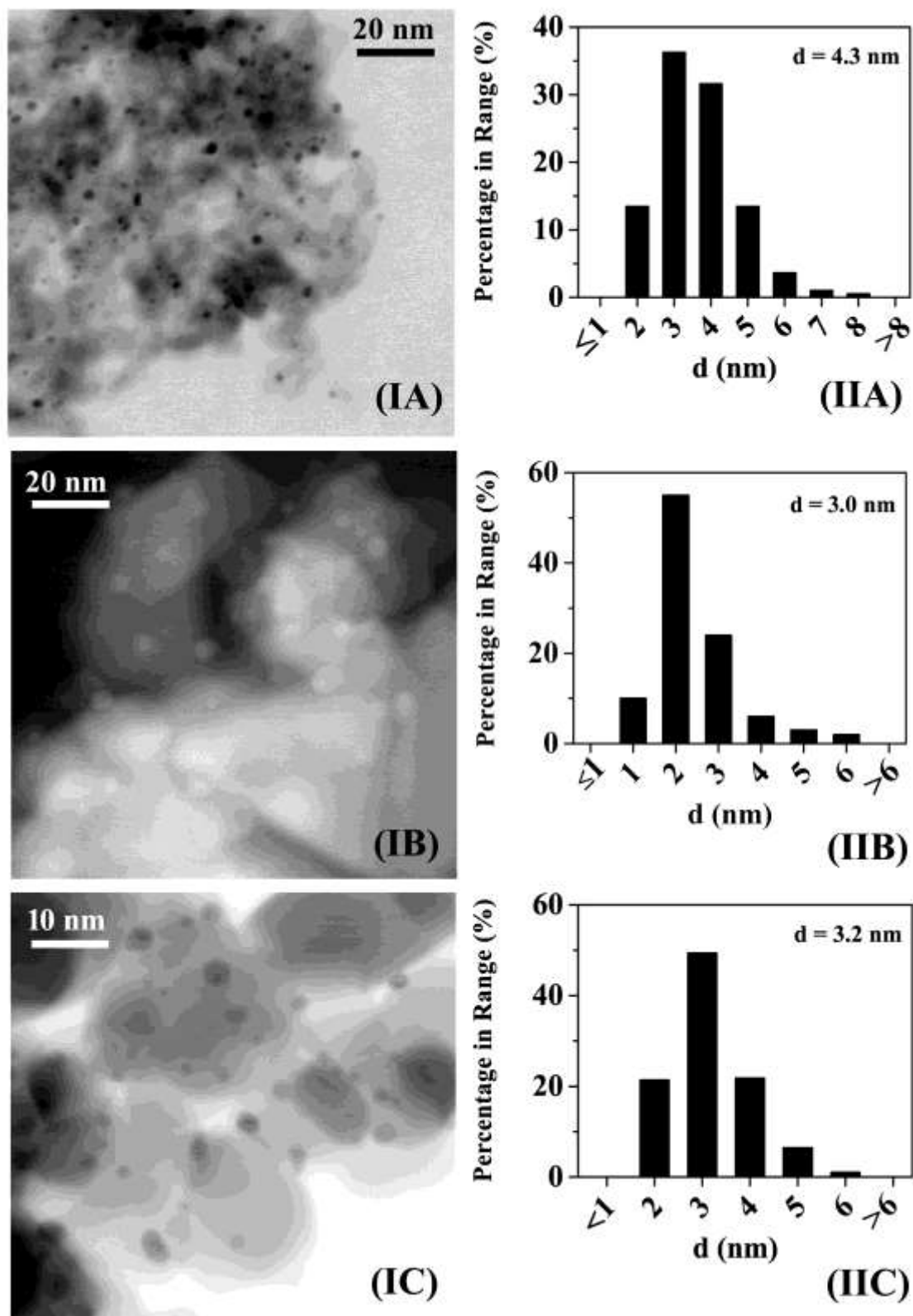


Figure 4

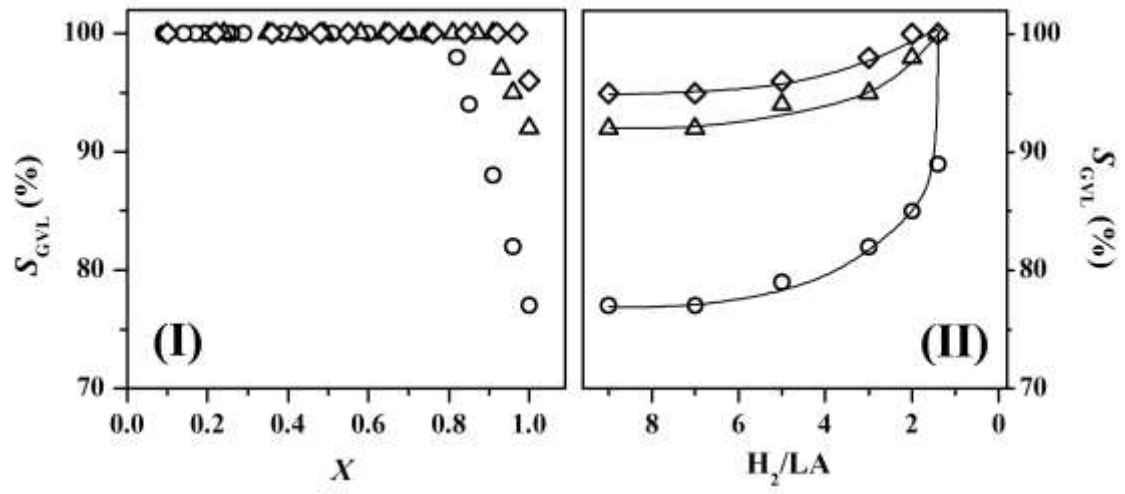


Figure 5

